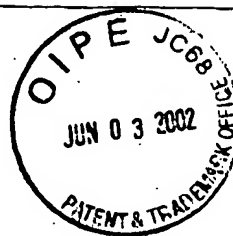


Exhibit 3

Genest, Margaret M.

From: Jeff Koberstein [jk1191@columbia.edu]
Sent: Wednesday, April 17, 2002 3:22 PM
T : Genest, Margaret M.
Subject: Re: signature requested



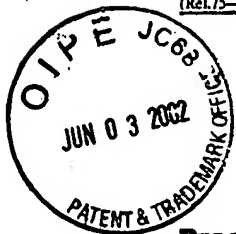
I am not inclined at present to sign the Power of Attorney until I have adequate time to consider the implications of such an action. I do not have time in the near future to complete such consideration.
Jeff Koberstein

At 11:55 AM 4/17/02 -0400, you wrote:

>Hi Dr. Koberstein,

>I was checking to make sure that I clearly understand the conversation we
>had on Monday morning, April 15, regarding the signature I was requesting
>from you for your patent application. You stated that because of some other
>issues with the University of CT you were not going to sign the Declaration
>and Power of Attorney document that was sent to you. You also said that
>because of a recent move from your office you had not even opened the
>envelope that was from UConn. Please confirm that my understanding of the
>situation is correct. Thank you, Margaret
>

Prof. Jeffrey T. Koberstein
Department of Chemical Engineering and Applied Chemistry
Columbia University
500 West 120th Street, MC4721
New York, NY 10027
Tel. 212-854-3120 (office)
FAX 212-854-3054
email: jk1191@columbia.edu



Practitioner's Docket No. UConn 98-2163-P

**ADDED PAGE TO COMBINED DECLARATION
AND POWER OF ATTORNEY FOR SIGNATURE BY JOINT INVENTOR(S)
ON BEHALF OF NONSIGNING INVENTOR(S) WHO REFUSE(S)
TO SIGN OR CANNOT BE REACHED (37 CFR 1.47(a))**

WARNING: "37 C.F.R. § 1.47(a) and 35 U.S.C. § 116 ¶ 2 require all available joint inventors to file an application 'on behalf' of themselves and on behalf of a joint inventor who 'cannot' be found or reached after diligent effort" "or who refuses to 'join in an application.'" M.P.E.P. § 409.03(a), 6th ed., rev. 3 (emphasis added). See also 62 Fed. Reg. 53,131, 53,137, 203 O.G. 68 (Oct. 10, 1997).

I. I am an above named joint inventor and have signed this declaration on my own behalf and also sign this declaration under 37 CFR 1.47(a) on behalf of the nonsigning joint inventor, particulars for whom are:

Full name of (first, second, etc.) Jeffrey Koberstein
nonsigning inventor who

- ☒ refuses to sign
☐ cannot be found or reached

NOTE: The name of the nonsigning inventor(s) should preferably also be filled in at the appropriate prior space in the declaration, adding the words "nonsigning inventor-completed on added page."
United States

Country of Citizenship of nonsigning inventor
116 Wildwood Road, Storrs, CT 06268

Last known address of nonsigning inventor

NOTE: Ordinarily, the last known address will be the last known residence of the nonsigning inventor(s). A post office box is insufficient. Other addresses at which the nonsigning inventor(s) may be reached should also be given. These can best be given in the Statement Of Facts In Support Of Filing On Behalf Of Omitted Inventor. MPEP § 409.03(e), 6th ed.

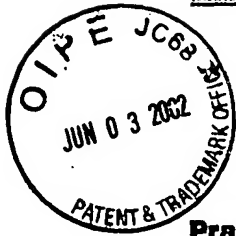
II. Accompanying this declaration is:

- (1) A STATEMENT OF FACTS IN SUPPORT OF FILING ON BEHALF OF NONSIGNING INVENTOR
- (2) THE PETITION FEE OF \$130.00 (37 CFR 1.17(i))

Francis Moussy

(type or print name of joint inventor
signing on behalf of nonsigning
inventor)


Signature



Practitioner's Docket No. UConn 98-2163-P

**ADDED PAGE TO COMBINED DECLARATION
AND POWER OF ATTORNEY FOR SIGNATURE BY JOINT INVENTOR(S)
ON BEHALF OF NONSIGNING INVENTOR(S) WHO REFUSE(S)
TO SIGN OR CANNOT BE REACHED (37 CFR 1.47(a))**

WARNING: "37 C.F.R. § 1.47(a) and 35 U.S.C. § 116 ¶ 2 require all available joint inventors to file an application 'on behalf' of themselves and on behalf of a joint inventor who 'cannot' be found or reached after diligent effort" "or who refuses to 'join in an application.'" M.P.E.P. § 409.03(a), 6th ed., rev. 3 (emphasis added). See also 62 Fed. Reg. 53,131, 53,137, 203 O.G. 68 (Oct. 10, 1997).

I. I am an above named joint inventor and have signed this declaration on my own behalf and also sign this declaration under 37 CFR 1.47(a) on behalf of the nonsigning joint inventor, particulars for whom are:

Full name of (first, second, etc.) Jeffrey Koberstein
nonsigning inventor who

- ☒ refuses to sign
☐ cannot be found or reached

NOTE: The name of the nonsigning inventor(s) should preferably also be filled in at the appropriate prior space in the declaration, adding the words "nonsigning inventor-completed on added page."
United States

Country of Citizenship of nonsigning inventor
116 Wildwood Road Storrs, CT 06268

Last known address of nonsigning inventor

NOTE: Ordinarily, the last known address will be the last known residence of the nonsigning inventor(s). A post office box is insufficient. Other addresses at which the nonsigning inventor(s) may be reached should also be given. These can best be given in the Statement Of Facts In Support Of Filing On Behalf Of Omitted Inventor. MPEP § 409.03(e), 6th ed.

II. Accompanying this declaration is:

- (1) A STATEMENT OF FACTS IN SUPPORT OF FILING ON BEHALF OF NONSIGNING INVENTOR
(2) THE PETITION FEE OF \$130.00 (37 CFR 1.17(f))

Donald Kreutzer

(type or print name of joint inventor
signing on behalf of nonsigning
inventor)

Signature

Practitioner's Docket No. UConn 98-2163-P

**ADDED PAGE TO COMBINED DECLARATION
AND POWER OF ATTORNEY FOR SIGNATURE BY JOINT INVENTOR(S)
ON BEHALF OF NONSIGNING INVENTOR(S) WHO REFUSE(S)
TO SIGN OR CANNOT BE REACHED (37 CFR 1.47(a))**

WARNING: "37 C.F.R. § 1.47(a) and 35 U.S.C. § 116 ¶ 2 require all available joint inventors to file an application 'on behalf' of themselves and on behalf of a joint inventor who 'cannot' be found or reached after diligent effort" "or who refuses to 'join in an application.'" M.P.E.P. § 409.03(e), 6th ed., rev. 3 (emphasis added). See also 62 Fed. Reg. 53,131, 53,137, 203 O.G. 68 (Oct. 10, 1997).

I. I am an above named joint inventor and have signed this declaration on my own behalf and also sign this declaration under 37 CFR 1.47(a) on behalf of the nonsigning joint inventor, particulars for whom are:

Full name of (first, second, etc.) Jeffrey Koberstein
nonsigning inventor who

- ☒ refuses to sign
☐ cannot be found or reached

NOTE: The name of the nonsigning inventor(s) should preferably also be filled in at the appropriate prior space in the declaration, adding the words "nonsigning inventor-completed on added page."
United States

Country of Citizenship of nonsigning inventor
116 Wildwood Road Storrs, CT 06268

Last known address of nonsigning inventor

NOTE: Ordinarily, the last known address will be the last known residence of the nonsigning inventor(s). A post office box is insufficient. Other addresses at which the nonsigning inventor(s) may be reached should also be given. These can best be given in the Statement Of Facts In Support Of Filing On Behalf Of Omitted Inventor. MPEP § 409.03(e), 6th ed.

II. Accompanying this declaration is:

(1) A STATEMENT OF FACTS IN SUPPORT OF FILING ON BEHALF OF NONSIGNING INVENTOR

(2) THE PETITION FEE OF \$130.00 (37 CFR 1.17(l))

Diane Burgess

(type or print name of joint inventor
signing on behalf of nonsigning
inventor)

Signature

#3



Practitioner's Docket No. UConn 98-2163-P

**ADDED PAGE TO COMBINED DECLARATION
AND POWER OF ATTORNEY FOR SIGNATURE BY JOINT INVENTOR(S)
ON BEHALF OF NONSIGNING INVENTOR(S) WHO REFUSE(S)
TO SIGN OR CANNOT BE REACHED (37 CFR 1.47(a))**

WARNING: "37 C.F.R. § 1.47(a) and 35 U.S.C. § 116 ¶ 2 require all available joint inventors to file an application 'on behalf' of themselves and on behalf of a joint inventor who 'cannot' be found or reached after diligent effort" "or who refuses to 'join in an application.'" M.P.E.P. § 409.03(e), 6th ed., rev. 3 (emphasis added). See also 62 Fed. Reg. 53,131, 53,137, 203 O.G. 68 (Oct. 10, 1997).

I. I am an above named joint inventor and have signed this declaration on my own behalf and also sign this declaration under 37 CFR 1.47(a) on behalf of the nonsigning joint inventor, particulars for whom are:

Full name of (first, second, etc.) Jeffrey Koberstein
nonsigning inventor who

- ☒ refuses to sign
- ☐ cannot be found or reached

NOTE: The name of the nonsigning inventor(s) should preferably also be filled in at the appropriate prior space in the declaration, adding the words "nonsigning inventor-completed on added page."
United States

Country of Citizenship of nonsigning inventor
116 Wildwood Road Storrs, CT 06268

Last known address of nonsigning inventor

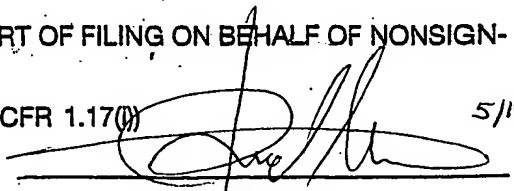
NOTE: Ordinarily, the last known address will be the last known residence of the nonsigning inventor(s). A post office box is insufficient. Other addresses at which the nonsigning inventor(s) may be reached should also be given. These can best be given in the Statement Of Facts In Support Of Filing On Behalf Of Omitted Inventor. MPEP § 409.03(e), 6th ed.

II. Accompanying this declaration is:

- (1) A STATEMENT OF FACTS IN SUPPORT OF FILING ON BEHALF OF NONSIGNING INVENTOR
- (2) THE PETITION FEE OF \$130.00 (37 CFR 1.17(b))

Fotios Papadimitrakopoulos

(type or print name of joint inventor
signing on behalf of nonsigning
inventor)


Signature

5/14/02

Practitioner's Docket No. UConn 98-2163-P

**ADDED PAGE TO COMBINED DECLARATION
AND POWER OF ATTORNEY FOR SIGNATURE BY JOINT INVENTOR(S)
ON BEHALF OF NONSIGNING INVENTOR(S) WHO REFUSE(S)
TO SIGN OR CANNOT BE REACHED (37 CFR 1.47(a))**

WARNING: "37 C.F.R. § 1.47(a) and 35 U.S.C. § 116 ¶ 2 require all available joint inventors to file an application 'on behalf' of themselves and on behalf of a joint inventor who 'cannot' be found or reached after diligent effort" "or who refuses to 'join in an application.'" M.P.E.P. § 409.03(e), 6th ed., rev. 3 (emphasis added). See also 62 Fed. Reg. 53,131, 53,137, 203 O.G. 68 (Oct. 10, 1997).

I. I am an above named joint inventor and have signed this declaration on my own behalf and also sign this declaration under 37 CFR 1.47(a) on behalf of the nonsigning joint inventor, particulars for whom are:

Full name of (first, second, etc.) Jeffrey Koberstein
nonsigning inventor who

- ☒ refuses to sign
☐ cannot be found or reached

NOTE: The name of the nonsigning inventor(s) should preferably also be filled in at the appropriate prior space in the declaration, adding the words "nonsigning inventor-completed on added page."
United States

Country of Citizenship of nonsigning inventor
116 Wildwood Road Storrs, CT 06268

Last known address of nonsigning inventor

NOTE: Ordinarily, the last known address will be the last known residence of the nonsigning inventor(s). A post office box is insufficient. Other addresses at which the nonsigning inventor(s) may be reached should also be given. These can best be given in the Statement Of Facts In Support Of Filing On Behalf Of Omitted Inventor. MPEP § 409.03(e), 6th ed.

II. Accompanying this declaration is:

- (1) A STATEMENT OF FACTS IN SUPPORT OF FILING ON BEHALF OF NONSIGNING INVENTOR
- (2) THE PETITION FEE OF \$130.00 (37 CFR 1.17(l))

Samuel Huang
(type or print name of joint inventor
signing on behalf of nonsigning
inventor)

Samuel Huang, 5/10/02
Signature

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re application of: Moussey et al.

For: APPARATUS AND METHOD FOR CONTROL OF TISSUE/IMPLANT INTERACTIONS

the specification of which:

(check and complete (a), (b), or (c))

- (a) ☐ is attached hereto.
- (b) ☒ was filed on 01/31/02, as Application Serial No. 0 / 10/066,393
and was amended on _____ (if applicable).
- (c) ☐ was described and claimed in International Application No. _____
filed on _____ and as amended on _____ (if any).

**STATEMENT OF FACTS IN SUPPORT OF FILING
ON BEHALF OF NONSIGNING INVENTOR (37 C.F.R. § 1.47)**

NOTE: This statement as to the pertinent facts concerning the refusal of the nonsigning inventor to join in the application or where the omitted inventor cannot be found or reached must accompany the declaration signed on behalf of the omitted inventor by a joint inventor or by a legal representative who shows a proprietary interest. Where the entity with a proprietary interest executes the declaration on behalf of the omitted inventor there must also be a showing that such action is necessary to preserve the rights of the parties or to prevent irreparable damage. 37 C.F.R. §§ 1.47(a) and (b).

This statement is made as to the exact facts that are relied upon to establish the diligent effort made to secure the execution of the declaration by the nonsigning inventor for the above-identified patent application before deposit thereof in the Patent and Trademark Office.

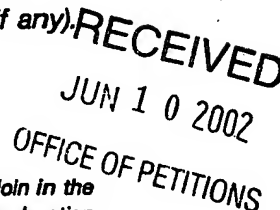
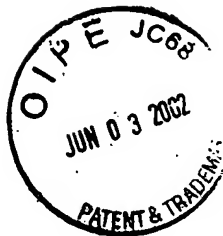
(check next item, if applicable)

- ☐ Because signing on behalf of the nonsigning inventor is by a person or entity showing a sufficient proprietary interest, this statement also recites facts as to why this action was necessary to preserve the rights of the parties or to prevent irreparable damage.

This statement is being made by the available person having first-hand knowledge of the facts recited therein.

NOTE: The statement "must be signed, where at all possible, by a person having first-hand knowledge of the facts recited therein." M.P.E.P. § 409.03(d), 7th ed. If different persons have first-hand knowledge of different facts, then a declaration from each such person as to those facts he or she knows should be submitted separately.

NOTE: Copies of documentary evidence, such as certified mail return receipt, cover letter of instructions, telegrams, etc., that support a finding that the nonsigning inventor could not be reached should be made part of the affidavit or declaration. It is important that the affidavit or declaration contain statements of fact as opposed to conclusions. M.P.E.P. § 409.03(d), 7th ed.



LAST KNOWN ADDRESS OF THE NONSIGNING INVENTOR

NOTE: The last known address of the nonsigning inventor must be stated so that the PTO can forward the notice of filing of the application to the nonsigning inventor at said address. (37 C.F.R. § 1.47). A post office box is insufficient. M.P.E.P. § 409.03(e), 6th ed.

Jeffrey Koberstein

Full name of nonsigning inventor

116 Wildwood Road, Storrs, CT 06268

Last known address of nonsigning inventor

NOTE: Ordinarily, the last known address will be the last known residence of the nonsigning inventor, but other addresses at which the nonsigning inventor may be reached should also be given in the space below. M.P.E.P. § 409.03(e), 6th ed.

Jeffrey Koberstein
Columbia University
Mudd Building Room 812
500 West 120th Street
MC 4721
New York, NY 10027

IDENTIFICATION OF PERSON MAKING THIS STATEMENT OF FACTS

Kim Post
Name
11 Fisk Avenue
Address
Stafford Springs, CT 06076

(Statement of Facts in Support of Filing on Behalf of Nonsigning Inventor [1-6]—page 2 of 8)

DETAILS OF REFUSAL OF NONSIGNING INVENTOR TO SIGN APPLICATION PAPERS



NOTE: Complete either these facts or the facts as to **DETAILS OF EFFORTS TO REACH NONSIGNING INVENTOR.**

NOTE: The circumstances of this refusal must be specified by the person to whom the refusal was made and, before a refusal can be alleged, it must be demonstrated that a bona fide attempt was made to present a copy of the application papers (specification, including claims, drawings and declaration) to the nonsigning inventor for signature. A copy of the application papers should be sent to the last known address of the nonsigning inventor, or, if the nonsigning inventor is represented by counsel, to the address of the nonsigning inventor's attorney. The time and place of an oral refusal should be stated, or a copy of the written refusal should be attached.

If it is the conduct as a whole of the nonsigning inventor that is the refusal, then all the facts upon which this conclusion is based should be stated and a copy of any documentary evidence supporting these facts should be attached.

Where there is an express oral refusal, that fact along with the time and place of the refusal must be stated in the affidavit or declaration. When there is an express written refusal, a copy of the document evidencing that refusal must be made part of the affidavit or declaration.

Whenever the nonsigning inventor gives a reason for refusing to sign the application papers, that reason should be stated. M.P.E.P. § 19.03(a), 7th ed.

1. Somewhere near the end of March I received documents from Margaret Genest to forward to Jeffrey Koberstein for his signature.

2. I sent the documents to Dr. Koberstein some time at the end of March. I sent them to:

Jeffrey Koberstein
Columbia University
Mudd Building Room 812
500 West 120th Street
MC 4721
New York, NY 10027

Date signed: 5-24-02


Signature
Kim Post

UCT 98-2163P



Express Mail Label No: EL 835033981 US

APPARATUS AND METHOD FOR CONTROL
OF TISSUE/IMPLANT INTERACTIONS

Cross-Reference to Related Application

This application claims the benefit of U.S. Application Serial No. 09/443,857 filed November 19, 1999, which claims the benefit of U.S. Provisional Application No. 60/109,289, filed November 20, 1998, which are incorporated by reference herein in their entirety.

5

Background of the Invention

1. Field of the Invention

This invention relates generally to the field of implants for human and animal bodies. In particular, this invention relates to apparatus and methods for controlling tissue/implant interactions, thereby allowing better integration, function, and extended lifespan of implants in the body.

10

2. Description of the Related Art

Implantable artificial materials and devices, such as drug delivery systems, pacemakers, artificial joints, and organs play an important role in health care today. In addition to these devices, implantable monitoring "devices or "biosensors" have great potential for improving both the quality of care and quality of life of patients and animals. An exemplary monitoring device that would greatly improve the quality of life for diabetic patients and animals, for example, is an implantable glucose monitor for the pain-free, continuous, reliable monitoring of blood glucose levels. Diabetic patients presently monitor their own glucose blood levels by obtaining samples of capillary blood through repeated finger-pricking. Because the tests are painful, time-consuming, and must be performed multiple times throughout a single day, diabetic patients resist performing an adequate number of daily tests. This low compliance exacerbates the intrinsically discontinuous nature

15

20

of the monitoring, and ultimately leads to the extensive pathology associated with diabetic patients.

One of the major problems associated with all types of implants is biocompatibility of the implant with the body, and in particular with the tissue adjacent to the site of the implant.

For example, despite attempts to design implantable biosensors for glucose and other monitoring functions, none developed to date provide pain-free, reliable and continuous monitoring. One reason is that current implantable sensors suffer from a progressive loss of function after relatively short periods of time *in vivo*. This loss in function arises from multiple factors, some of the most important of which include protein adsorption,

inflammation, and fibrosis (encapsulation) resulting from tissue trauma at the site of the implant. This fibrosis results in loss of blood vessels at the site of implantation and therefore in a reduced access to blood glucose levels. These factors can also interfere with the function of other implants and implantable devices, such as insulin pumps, pacemakers, artificial joints, and artificial organs.

One approach to control the inflammation and fibrosis resulting from tissue trauma at the site of implantation has been to use inert materials such as titanium or single-crystalline alumina, as disclosed in U.S. Patent No. 4,122,605 to Hirabayashi et al. While suitable for bone or tooth implants, this approach is not useful in more complex prosthetic devices or in biosensors, which requires use of a variety of materials. Another approach has been the use of a porous, outer coating of DACRON or TEFLON, as disclosed in U.S. Patent No. 4,648,880 to Brauman et al., or with polytetrafluorethylene, as disclosed in U.S. Patent No. 5,779,734. While suitable for prostheses such as breast implants, such coatings are not practical for prosthetic devices or biosensors having complex geometries. The most commonly-used approach to control tissue responses, particularly inflammation, has been the systemic administration of drugs such as corticosteroids. Such systemic administration can result in side effects such as generalized immunosuppression, bloating, and psychiatric problems, especially over the long term. There accordingly remains a need for both apparatus and methods for controlling tissue/implant interactions, particularly for implantable materials, prostheses, and devices such as biosensors.

Summary of the Invention

The above discussed and other drawbacks and deficiencies of the prior art are overcome or alleviated by an improved tissue/implant interface, comprising an implant having an outer surface and a bioactive polymer layer adjacent to at least a portion of the outer surface of the implant. In a preferred embodiment, the polymer layer contains at least one tissue response modifier covalently attached to the polymer layer or entrapped within the polymer layer in a quantity effective to control the tissue response at the site of implantation. The bioactive polymer layer may be a synthetic organic polymer such as a hydrogel, or a natural polymer such as a protein. The polymer may also be self-assembled. Preferably, the at least one tissue response modifier controls inflammation, fibrosis, cell migration, cell proliferation, leukocyte activation, leukocyte adherence, lymphocyte activation, lymphocyte adherence, macrophage activation, macrophage adherence, cell death and/or neovascularization. Exemplary tissue response modifiers include, but are not limited to, steroidal and non-steroidal anti-inflammatory agents, anti-fibrotic agents, anti-proliferative agents, cytokines, cytokine inhibitors, neutralizing antibodies, adhesive ligands, metabolites and metabolic intermediates, DNA, RNA, cytotoxic agents, and combinations thereof. The tissue response modifiers may be covalently attached to the polymer layer or entrapped within the polymer layer.

In another embodiment, the tissue response modifier is covalently attached to the polymer layer or entrapped within the polymer layer in slow-release form, for example in the form of biodegradable polymers, nanoparticles, liposomes, emulsions, and or microspheres, to provide long-term delivery of the tissue response modifier to the site of implantation. Preferably, at least a portion of the microspheres have been treated to enhance release rate of the tissue response modifier.

The addition of the various combinations of tissue response modifiers with bioactive polymers provides an extremely simple, flexible and effective means to control the implant/tissue interphase, improving implant lifetime and function. The above-discussed and other features and advantages will be appreciated and understood by those skilled in the art from the following detailed description and drawings.

Brief Description of the Drawings

Referring now to the drawings wherein like elements are numbered alike in the several FIGURES:

FIGURE 1 is a schematic representation of an implant and tissue response modifier-hydrogel combination.

FIGURE 2 is a schematic representation of an implant and tissue response modifier-MAP-poly(anion/polycation) combination.

FIGURE 3 is a schematic representation of a hydrogen peroxide-based amperometric sensor for monitoring subcutaneous levels of glucose and bioactive layer interface.

FIGURE 4 is a detail of FIG. 3.

FIGURE 5 is a graph showing the permeability of a HEMA-FOSA hydrogel to glucose.

FIGURE 6 is a graph showing ellipsometrically determined thickness versus dip cycle for alternating NAFIONTM/Fe³⁺ assemblies as a function of the pH of NAFIONTM solution; (A) pH = 3, (B) pH = 4.5, and (C) pH = 5.5.

FIGURE 7 is a graph showing ellipsometrically determined thickness versus dip cycle for alternating NAFIONTM/Fe³⁺ assemblies as a function of the pH and ionic strength of NAFIONTM solution: (A) pH = 3, 0.01 M KCl; (B) pH = 3, no salt; (C) pH = 4.5, 0.01 M KCl; (D) pH = 4.5, no salt.

FIGURE 8 is a graph showing glucose permeability data as a function of successive NAFIONTM/Fe³⁺ self assembled monolayers on a 0.1 micron glass-fiber membrane.

FIGURE 9 shows Quartz Crystal Microbalance (QCM) frequency shifts (directly related with the mass deposited on the QCM sensor) versus dip cycle for humic acid/Fe³⁺ assemblies, as a function of the pH and ionic strength of humic acid solutions.

FIGURE 10 is a graph showing ellipsometrically determined thickness versus dip cycle for humic acid/Fe³⁺ assemblies, as a function of the pH and ionic strength of humic acid solutions.

FIGURE 11 shows SEM images of standard and predegraded microspheres; (A and C) are standard microspheres and (B and D) are predegraded microspheres. (A and B) are high magnification images and (C and D) are low magnification images.

FIGURE 12 is a graph showing dexamethasone degradation with time.

FIGURE 13 is a graph showing a dexamethasone degradation function.

FIGURE 14 is a graph showing cumulative dexamethasone release from standard microspheres during in vitro release.

FIGURE 15 is a graph showing cumulative dexamethasone release from predegraded microspheres during in vitro release.

FIGURE 16 is a graph showing cumulative dexamethasone release from mixed standard and predegraded microspheres during in vitro release.

FIGURE 17 is a graph showing cumulative dexamethasone release from PLGA microspheres with 10% (w/w) PEG added during in vitro release.

FIGURE 18 shows release profiles of dexamethasone from PVA hydrogels subjected to 3 (●), 4 (▲) or 5 (■) freeze-thaw cycles.

FIGURE 19 shows release profiles of dexamethasone from microspheres entrapped within PVA hydrogels. The symbols are: dexamethasone microspheres in a PVA hydrogel (□), dexamethasone microspheres in a PVA hydrogel with acrylic acid (△), dexamethasone microspheres in a PVA hydrogel with humic acid (X), dexamethasone microspheres in a PVA hydrogel with Nafion (○), and dexamethasone microspheres (◇).

Detailed Description of the Preferred Embodiments

As used herein, "implant" refers broadly to any material or device which is invasively inserted within the body of a vertebrate, e.g., bird, reptile, amphibian, or mammal. The improved tissue/implant interface of the present invention comprises, in a first embodiment, an implant having an outer surface and a bioactive polymer layer adjacent to at least a portion of the outer surface of the implant, wherein the polymer layer contains at least one tissue response modifier covalently attached to the polymer layer or entrapped within the polymer layer in a quantity effective to control the tissue response at the site of implantation. The at least one tissue response modifier serves to modify tissue response to the implant at the site of implantation, moderating or preventing the tissue responses which lead to implant rejection, impairment, or loss of function.

“Tissue response modifiers” as used herein are factors that control the response of tissue adjacent to the site of implantation. One facet of this response can be broadly divided into a two-step process, inflammation and wound healing. An uncontrolled inflammatory response (acute or chronic) results in extensive tissue destruction and ultimately tissue fibrosis. Wound healing includes regeneration of the injured tissue, repair (fibrosis), and ingrowth of new blood vessels (neovascularization and angiogenesis). For fibrosis, the body utilizes collagen from activated fibroblasts to “patch and fill” the unregenerated areas resulting from trauma and inflammation. Ingrowth of new blood vessels is critical to the ultimate outcome of wound healing. A number of other responses are also included within this category, for example fibroblast formation and function, leukocyte activation, leukocyte adherence, lymphocyte activation, lymphocyte adherence, macrophage activation, macrophage adherence, thrombosis, cell migration, cell proliferation including uncontrolled growth, neoplasia, and cell injury and death. Adverse tissue responses to implantation may also arise through genetic disorders, immune diseases, infectious disease, environmental exposure to toxins, nutritional diseases, and diseases of infancy and childhood.

Tissue response modifiers are therefore a broad category of organic and inorganic, synthetic and natural materials, and derivatives thereof which affect the above responses to tissue injury upon implantation. Such materials include but are not limited to synthetic organic compounds (drugs), peptides, polypeptides, proteins, lipids, sugars, carbohydrates, certain RNA and DNA molecules, and fatty acids, as well metabolites and derivatives of each. Tissue response modifiers may also take the form of, or be available from genetic material, viruses, prokaryotic or eukaryotic cells. The tissue response modifiers can be in various forms, such as unchanged molecules, components of molecular complexes, or pharmacologically acceptable salts or simple derivatives such as esters, ethers, and amides. Tissue response modifiers may be derived from viral, microbial, fungal, plant, insect, fish, and other vertebrate sources.

Exemplary tissue response modifiers include, but are not limited to, anti-inflammatory agents such as steroidal drugs, for example corticosteroids such as Dexamethasone (9-alpha-fluoro-16-alpha-methylprednisolone), a potent, broad spectrum steroidal anti-inflammatory and anti-fibrotic drug with known efficacy in a diabetic rat

model, methyl prednisone, triamcortolone (fluoroxyprednisolone), hydrocortisone (17-hydroxycorticosterone); and non-steroidal drugs, for example Ketoprofen (2-(3-benzophenyl)propionic acid), cyclosporin, Naproxen ((+)-6-methoxy- α -methyl-2-naphthalene acetic acid), and Ibuprofen (4-isobutyl- α -methylphenyl acetic acid).

5 Other exemplary tissue response modifiers include neovascularization agents such as cytokines. Cytokines are growth factors such as transforming growth factor alpha (TGFA), epidermal growth factor (EGF), vascular endothelial growth factor (VEGF), and anti-transforming growth factor beta (TGFB). TGFA suppresses collagen synthesis and stimulates angiogenesis. It has been shown that epidermal growth factor tethered to a solid
10 substrate retains significant mobility and an active conformation. VEGF stimulates angiogenesis, and is advantageous because it selectively promotes proliferation of endothelial cells and not fibroblasts or collagen synthesis, in contrast to other angiogenic factors. In addition to promoting wound healing, the improved blood flow resulting from the presence of neovascularization agents should also improve the accuracy of sensor measurements.

15 Another type of tissue response modifier is a neutralizing antibody including, for example, anti-transforming growth factor beta antibody (anti-TGFB); anti-TGFB receptor antibody; and anti-fibroblast antibody (anti-CD44). Anti-TGFB antibody has been shown to inhibit fibroblast proliferation, and hence inhibit fibrosis. Because of the importance of TGFB in fibrosis, anti-TGFB receptor antibodies inhibit fibrosis by blocking TGFB
20 activation of fibroblasts. Recent studies have demonstrated that anti-CD44 antibody induces programmed cell death (apoptosis) in fibroblasts in vitro. Thus, use of anti-CD44 antibody represents a novel approach to inhibition of fibroblast formation, and therefore fibrosis. Other anti-proliferative agents include Mitomycin C, which inhibits fibroblast proliferation under certain circumstances, such as after vascularization has occurred.

25 Adhesive ligands ("binding motifs") may also be used as tissue response modifiers, wherein the adhesive ligands are incorporated into the polymer layer to stimulate direct attachment of endothelial cells to implant surfaces. Such attachment promotes neovascularization at the implant/tissue interface. Where the surface density of binding motifs has an effect on the cellular response, variation in the density of the binding motifs
30 allows control of the response. Exemplary adhesive ligands include but are not limited to the

arginine-glycine-aspartic acid (RGD) motif, and arginine-glutamic acid-aspartic acid-valine (REDV) motif, a fibronectin polypeptide. The REDV ligand has been shown to selectively bind to human endothelial cells, but not to bind to smooth muscle cells, fibroblasts or blood platelets when used in an appropriate amount.

5 The at least one tissue response modifier is covalently bound to or entrapped within at least one bioactive polymer layer. As used herein, a "bioactive" polymer layer is one which can control (enhance or suppress) tissue reactions to implanted materials.

 The bioactive polymers are generally biocompatible, that is, physiologically tolerated and not causing adverse local or systemic responses. It is to be understood that the term
10 "layer" as used herein is inclusive of blocks, patches, semicircles, and other geometries without limitation. While synthetic polymers such as poly(tetrafluoroethylene), silicones, poly(acrylate), poly(methacrylate), hydrogels, and derivatives thereof are most commonly used, natural polymers such as proteins and carbohydrates are also within the scope of the present invention. The bioactive polymer layer functions to protect the implant and preserve
15 its function, minimize protein adsorption of the implant, and serve as a site for the delivery of the tissue response modifiers or drug delivery vehicles.

 In one embodiment, the tissue response modifiers are entrapped or covalently bound within a hydrogel. Hydrogels are formed from the polymerization of hydrophilic and hydrophobic monomers to form gels and are described, for example, in U.S. Patent No.
20 4,983,181 and No. 4,994,081, which are incorporated by reference herein. They consist largely of water, and may be crosslinked by either chemical or physical methods. Chemical crosslinking is exemplified by the free-radical induced crosslinking of dienes such as ethylene glycol dimethacrylate (EGDMA), and the like. Physical crosslinks are formed by copolymerizing a hydrophobic co-monomer with the water-soluble monomer, and then by
25 contacting the copolymerized gel with water. Physical association of the hydrophobic regions of the gel results in the formation of physical crosslinks. Control of the ratio of hydrophilic to hydrophobic monomers allows control of the final properties of the gel. Physical crosslinks can also be formed by freeze/thaw methods, for example freeze/thawing a poly(vinyl alcohol) (PVA) hydrogel as described below. Highly water-swollen hydrogels are
30 bioactive, and have minimal impact on the diffusion rates of small molecules. Hydrogels are

also intrinsically mobile, and therefore have minimal deleterious effects on associated peptide tissue response modifiers.

Hydrogels may be formed by the polymerization of monomers such as 2-hydroxyethyl methacrylate, 2-hydroxyethyl methacrylate, fluorinated acrylates, acrylic acid, and methacrylic acid, and combinations thereof. Preferred hydrogels are copolymers of 2-hydroxyethyl methacrylate, wherein the co-monomers are selected to improve mechanical strength, stability to hydrolysis, or other mechanical or chemical characteristics.

Copolymerization with various acidic monomers can decrease the buffer capacity of the gel and thus modulate the release of the tissue response modifier. Preferred co-monomers

include, but are not limited to, 3-hydroxypropyl methacrylate, N-vinyl pyrrolidinone, 2-hydroxyethyl acrylate, glycerol methacrylate, n-isopropyl acrylamide, N,N-dimethylacrylamide, glycidyl methacrylate, and combinations thereof. Particularly preferred hydrogels are terpolymers of 2-hydroxyethyl methacrylate (HEMA), N-vinyl pyrrolidinone (NVP), and 2-N-ethylperfluorooctanesulfonamido ethyl acrylate (FOSA) with added

EGDMA to provide controlled crosslinking. HEMA is hydrophilic, and swells in the presence of water. The hydroxyl groups of HEMA also provide potential sites for the covalent attachment of tissue response modifiers, slow release delivery systems, and the like.

Acrylic acid, methacrylic acid, and other functionalized vinyl monomers can also be employed to provide these attachment sites. NVP is amphiphilic, wherein the backbone ring provides hydrophobicity and the polar amide group provides hydrophilicity. Poly(vinyl pyrrolidinone) is water soluble, physiologically inactive, and forms complexes with a number of small molecules such as iodine and chlorhexidine. Use of NVP improves the toughness of polymerized HEMA, and provides for the enhanced solubility of the other monomers under bulk polymerization conditions.

Polymerization methods known in the art may be used, depending on the implant. Thus, for implants capable of tolerating increased temperatures, polymerization may be initiated by heat in the presence of initiator such as azobisisobutyronitrile (AIBN). Photoinitiation by UV light may be used in the presence of initiators such as benzoin or benzil, and by visible light in the presence of initiators such as Eosin. Binding of the

hydrogel to the implant may be by mechanical forces, as the sheath around the implant formed during preparation of the hydrogel shrinks considerably during polymerization.

In a preferred embodiment, the rate of release of the tissue response modifier is further be modified by varying the composition and/or physical characteristics of the polymer layer. For example, alternative freeze/thawing of PVA physically crosslinks the PVA chains excluding water molecules. The number of freeze/thaw cycles controls the degree of crosslinking. PVA polymers prepared this way are biologically inert and have a close resemblance to human tissue, making them an exemplary material for biomedical applications. The larger the number of freeze/thaw cycles of the PVA polymer, the higher the level of crosslinking (C.M. Hassan and N.A. Peppas, in *Advances in Polymer Science*, Vol. 153, pages 37-65 (2000)). Thus, treatment of the polymer layer as well as modification of its composition can be used to adjust the release of the tissue response modifier.

In still another preferred embodiment, the tissue response modifiers are associated with a bioactive polymer layer that is generated by supramolecular self-assembly. Generation of materials by self-assembly has resulted in significant advances in the area of thin films, for example, wherein the sequential layering of (poly)cations/(poly)anions has allowed the incorporation of molecular dyes, nanocrystals, microspheres, charged proteins, and cell-growth factors into larger structures. Such layer-by-layer growth of small and large molecular weight compounds offers a high degree of flexibility in the construction of these more complex structures.

Electrostatic self-assembly is based on the attraction of oppositely charged species that render the "complex" insoluble to the mother solutions. This technique offers a powerful tool for building a variety of layer and multilayer structures from poly(anions) and poly(cations). These "fuzzy" nanoassemblies exhibit significant intermixing of the opposite charged polyion chains. The strong metal-ligand forces that stabilize self-assemblies give rise to physically-crosslinked structures. These systems are very stable even at low pH and in polar solvents, eliminating the need for chemical-crosslinking to provide dimensional stability. Assembly may occur directly on the implant, or adjacent a hydrogel membrane, providing a greater number of options for the development of the membranes and interactive surface hydrogels. The layer thickness and other microstructural characteristics of these

assemblies are sensitive to the type of charged species, their concentration, pH, molecular weight, ionic strength and the like.

An example of a bioactive layer generated by self-assembly is the formation of NAFIONTM/Fe³⁺ multilayer films. NAFIONTM is a perfluorinated electrolyte having sulfonic acid functionalities that has been previously used as a semipermeable membrane for electrochemical sensors. However, the strong ion-exchange properties of NAFIONTM lead to calcification *in vitro* and *in vivo*. The sulfonate (R-SO₃) groups present in the hydrophilic domains of the membrane act as nucleating sites for deposition of calcium phosphate. These crystals tend to inhibit metabolite transport through the membrane, and also embrittle the membrane, causing it to crack.

Electrostatic assembly of NAFIONTM and Fe³⁺ from dilute solutions of ferric citrate at a pH about 2 to 6 can be used to prevent calcium deposition. Layer-by-layer assembly allows gradual stress relaxation and complete substitution of NAFION's protons with Fe³⁺, thus inactivating all of the calcification nucleation sites. Use of ferric citrate solutions at a mild pH (e.g., at about 6) allows assembly of the membranes without protein, enzyme, or other tissue response modifier inactivation. Accordingly, upon immersion into the acidic NAFIONTM solution (pH about 3), substrate hydroxyl groups, i.e., silanol groups (Si-OH) are partially protonated, providing a strong electrostatic force to attract the negatively charged NAFIONTM micelles. After rinsing in water to remove loosely bound species, the substrate is dipped into ferric chloride solution. Ferric ions are attracted by the sulfonate groups, facilitating the surface charge reversal thereby restoring the original surface charge. The entire process is repeated until the desired thickness is achieved.

Another poly(ligand) useful for self-assembly is a mussel adhesive protein (MAP). Self-assembly of biological materials such as mussel adhesive proteins allows the incorporation of materials, which improve implant biocompatibility. MAP produced by the blue seal mussel (*Mytilus edulis*) generally comprises 75 to 85 repeating decameric units having the primary sequence of KPSY-Hyp-Hyp-T-DOPA, wherein Hyp is hydroxyproline and DOPA is 3,4-dihydroxyphenylalanine. DOPA is a strong metal chelating agent, particularly with Ca²⁺ and Fe³⁺, and the strong self-aggregation of DOPA in the presence of cations results in supra-molecular self-assembly. Accordingly, a substrate comprising metal

chelating groups, for example free amine groups, is sequentially immersed first, in a solution comprising metal ions (i.e. Ca^{2+} and/or Fe^{3+}) (followed by optional washing in fresh solvent); and second, in a solution comprising the poly(ligand) (i.e. the MAP protein) (followed by optional washing in fresh solvent). The thickness of the membrane will be directly
5 proportional to the number of sequential immersion cycles. The assembly of the membrane is monitored with Variable Angle Spectroscopic Ellipsometry (VASE), UV-VIS and Quartz Crystal Microbalance. The strong chelation between Ca^{2+} and DOPA in the MAP membrane results in a substantial decrease in porosity, allowing the permeation of small molecules such as glucose and oxygen, while excluding permeation of larger molecules. Additionally, the
10 introduction of small amount of crosslinking, via the Michael addition from neighboring lysine repeats by slight increase of pH above 8.5, may be used to further fine-tune the permeability of such assemblies to levels.

A major advantage of MAP is that it is not expected to calcify, as it has been shown that the lack of strong ionic forces (i.e. the weak acidity of DOPA moieties) and of nucleating
15 surfaces in these assemblies inhibits the growth of phosphate deposits in sea water, thus allowing MAP to maintain its strong adhesive nature (low glass transition temperature). In addition, the use of Ca^{2+} ions in assemblies of mussel adhesive proteins will also contribute to the reversal of any Ca^{2+} concentration gradient within the implant/tissue interphase. The reversal of the Ca^{2+} concentration gradient, along with the weak acidity of DOPA moieties,
20 should act as a further deterrent in $\text{Ca}_3(\text{PO}_4)_2$ build-up in the MAP membrane. Resistance to calcification is evaluated both *in vitro* (in DMEM culture medium) and *in vivo* (subcutaneously in rats).

Humic acids may also be polymerized, or self-assembled into a bioactive layer. Humic acids or "humic substances" are heterogeneous, high-molecular weight organic acids
25 having a large proportion of DOPA, and are resistant to microbial degradation. The known ability of humic acids to donate and accept electrons from a variety of metals and organic molecules explains their capability to shuttle electrons between the humic-reducing microorganisms and the Fe(III)-Fe(II) oxide. It has been suggested that humic acids participate in a biological electron transfer as a result of the electron accepting ability of
30 quinone moieties when reduced to hydroquinones and vice-versa. This renders the

Fe³⁺/humic acid assembled membranes an attractive vehicle for the attachment of various kind of cells to the bioactive layer.

Higher order supramolecular hydrogel architectures may be assembled on top of the MAP or humic acid layers, employing the well studied poly(anion)/poly(cation) technology. Suitable poly(anions) include the salts of poly(glutamic acid), and its copolymers with other amino acids. Suitable poly(cations) include the salts of polylysine, and its copolymers with other amino acids. In another embodiment, the tissue-implant interface comprises more than one bioactive polymer layer. For example, a mussel adhesive protein layer may be first self-assembled onto the outer surface of the implant, followed by self-assembly of a (poly)anion/(poly)cation film. Alternatively, a NAFIONTM layer may be disposed between the sensor and a hydrogel layer. NAFIONTM, being a low surface energy polymer, is generally nonadherent with other synthetic organic polymers when placed in an aqueous environment. Standard procedures to modify the surface of the fluoropolymer such as poly(tetrafluoroethylene) are accordingly used to produce a functional NAFIONTM surface that can covalently bind another polymer layer. The most commonly used modifying agent is a sodium ion etching agent (available commercially as Tetra-Etch), which produces unsaturated hydrocarbon chains at the NAFIONTM surface. Bulk free radical polymerization of the unsaturated functional groups with the hydrogel monomers, e.g., results in adhesion to the NAFIONTM surface.

Other components may also be incorporated into the bioactive polymer layer, such as poly(ethylene oxide) (PEG), to minimize protein adsorption. Poly(ethylene oxide) is most readily incorporated into the hydrogel, for example, by co-polymerization of a vinyl monomer having poly(ethylene oxide) side chains, for example poly(ethylene glycol) methacrylate (which is commercially available from Aldrich Chemical Co.), or a divinyl-terminated poly(ethylene glycol) macromonomer. Copolymerization of HEMA and poly(ethylene glycol) methacrylate in the presence of AIBN yields a more flexible, unhydrated copolymer. The optimal molecular weight and content of poly(ethylene oxide) for each application can be determined by protein adsorption studies.

To provide further chemical functionality on the bioactive polymer layer, particularly a hydrogel layer, either polyvinyl alcohol or polyethylene imine may be employed as

macromolecular surfactants. Where hydroxyl functionalities are available, the coupling is promoted by tresylation. Poly(ethylene oxide) may also be grafted to hydroxyl groups on the surface of the polymer layer by tresylation coupling with Jeffamine, an amine-terminated poly(ethylene oxide) commercially available from Huntsman.

5 A further embodiment of the present invention is a tissue/implant interface consisting of an implant having an outer surface and a bioactive polymer, particularly one of the above-described hydrogels, MAP layers, or poly(anion)/poly(cation) layers disposed on the outer surface, wherein the presence of the bioactive polymer provides effective modification of the tissue response without use of an added tissue response modifier. In particular, use of one or
10 more of these layers alone, is expected to improve the biocompatibility, lifespan, and/or function of the implant.

Where used, association of the tissue response modifiers with the bioactive polymer layer may be by physical means, i.e., entrapment within the polymer layer, or by covalent attachment within the bioactive polymer layer and/or at the surface of the bioactive polymer
15 layer. Entrapment may occur at the time the layer is formed, or subsequently, i.e., by absorption of the tissue response modifier into the formed layer. By adjusting the degree of crosslinking of the layer, the rate of diffusion from the layer to the site of implantation can be controlled.

Covalent coupling, e.g., to the hydroxy functionality of the HEMA monomers in the
20 hydrogel or hydroxyl moieties of the MAP protein, can be advantageous in that the bound factor can still bind to cell surface receptors and contribute to signal transduction, but does not leach from the hydrogel or be endocytosed. Coupling of peptides to hydroxyl functionalities may be accomplished by known methods, for example by activation of the hydroxyl group of HEMA with tresyl chloride in the presence of triethylamine, followed by
25 reaction with the N-terminus of the peptide. For the adhesive ligand REDV, the GREDVY (glycine-arginine-glutamic acid-aspartic acid-valine-tyrosine) motif is used. The glycine moiety acts as a spacer, while the tyrosine moiety enables radioiodine binding assays for determination of the coupling efficiency. Since the swelling ratios of the hydrogels are highly dependent on the solvent employed, appropriate choice of solvents allows control of
30 the spatial distribution of the coupled factors. Use of a highly swelling solvent such as

dimethyl sulfoxide allows homogeneous distribution of the factor(s) throughout the hydrogel, while use of a low-swelling solvent such as dioxane results in the factor(s) being more or less confined to the surface of the hydrogel.

In still another embodiment, the tissue response modifiers are present in the bioactive polymer layer as part of a controlled release delivery system. Use of controlled release delivery systems allows controlled, site-specific delivery of the tissue response modifier to the implantation site, thus limiting biodegradation and reducing or eliminating systemic side effects, and improving the therapeutic response. Duration of action and dosage level are also adjustable, which is critical in controlling inflammation and fibrosis. Lower dosage levels are required for targeted delivery (as opposed to systemic administration), which lowers the cost of treatment.

Controlled release vehicles are known in the art, and most commonly comprise biodegradable linkages or forms that release the active agent upon degradation at the site of implantation. Exemplary controlled release vehicles include but are not limited to biodegradable polymers, nanoparticles, and controlled release vesicles such as liposomes and microspheres. Since many controlled release delivery systems can be manufactured to provide different release rates under the same conditions, in one embodiment, a single tissue response modifier may be provided at different release rates, to achieve a specific release profile. In another embodiment, the availability of a plurality of tissue response modifiers is regulated by the different release rates of the delivery systems.

Microspheres are particularly useful. Microspheres are micron-sized spherical articles, typically prepared using natural or synthetic polymers, and have been demonstrated to effectively deliver a number of drugs, including dexamethasone, and various proteins. To maximize control of the diverse and dynamic processes involved in inflammation, repair, and neovascularization, mixtures of microspheres comprising different tissue response modifiers may be used in combination. Additionally, microspheres are manufactured so as to release the various tissue response modifiers at different rates, to control the different phases of the tissue reaction. Microspheres having diameters from 1 to 100 microns, preferably 1 to 50 microns are suitable. Microspheres having diameters of greater than about 10 microns are presently preferred. The microspheres may be covalently attached to the implant or hydrogel,

or be physically entrained within the hydrogel. Coupling to the interactive hydrogels is by incorporation of different functional surfactants onto the surface of the microspheres.

Microsphere delivery systems may be encapsulating, having the active agent incorporated into the center, or have the active agent dispersed throughout the polymer matrix. Each microsphere is optimized for formulation method, release rate, and dosage of specific tissue response modifiers. Co-polymer ratio, particle size and drug loading are varied to achieve desired release rates of the tissue response modifiers. Since small microspheres are likely to be phagocytosed and removed from the site, preferred microspheres have diameters in the range from about 10 to about 100 microns. The method described by M. Tsung and D. J. Burgess, in J. Pharm., Vol. 86, p.603 (1997) may be used for particle sizing. SEM, TEM, and optical microscopy are used to determine microsphere size, shape, surface characteristics, and internal structure.

A number of polymers are suitable for use in slow release microspheres, including but not being limited to proteins, as disclosed in U.S. Patent No. 5,271,961, polyorthoesters, poly(lactic acid), poly(glycolic acid) polyahydrides, polyphosphazene, polycaprolactone, polyhydroxybutyrate and combinations thereof. A preferred polymer is poly(lactic-glycolic acid) ("PLGA"). PLGA is bioactive, does not itself result in any significant inflammatory reaction, can be manufactured to have different release rates, and is suitable for use with a variety of both water-soluble and water-insoluble drugs. PLGA microsphere preparations are commercially available under the trade name LUPRON-DEPOT[®] and are approved for use by the Federal Drug Administration (FDA) for parenteral administration. The ratio of glycolic acid to lactic acid, particle size, molecular weight of the polymer and drug loading are varied to achieve desired release rates of the tissue response modifiers.

Modification of the PLGA microsphere surface by tresylation allows covalent attachment of the microsphere to the hydroxyl groups of the hydrogel. Attachment of polyethylenamine or polyvinyl alcohol to the microsphere surface occurs by addition of these elements during microsphere preparation. These elements to allow coupling to the interactive surface hydrogels. Copolymerization of PLGA with a small amount of glutamic acid (approximately 5%) also allows coupling of the microspheres with the hydrogels.

Coating or modifying the surface of the PLGA microspheres also allows adjustment of biocompatibility, biodegradation, and release rates. Glutamic acid imparts a negative charge on the surface of the microspheres, allowing self assembly with the polypeptides. As an alternative, polyethyleneamine, phosphatidic acid or phosphatidylinositol attached to the microsphere surface imparts positive, negative, and negative charges, respectively. These elements become attached to the microsphere surface by incorporating them during microsphere preparation.

Preparation of microspheres comprising water-insoluble tissue response modifiers such as dexamethasone relies on the hydrophobicity of these molecules. A simple oil/water emulsion technique is used, wherein the dexamethasone, e.g., is entrapped within the internal oil phase (PLGA/methylene chloride) of the emulsion and hence within the microspheres following solvent evaporation, as described by C. Grandfils, et al., in J. Biomedical Materials Research, Vol. 26, p. 467 (1992). In order to increase dexamethasone content within the microspheres, dexamethasone partitioning into the aqueous phase is reduced by changing the oil phase, e.g. a methylene chloride/acetone mixture is used in place of methylene chloride. For hydrophilic tissue response modifiers such as VEGF and other polypeptides, a modification of a multiple emulsion technique described by Toguchi *et al.* in J. Pharm. Sci., Vol. 83, p. 636 (1994) is used, since polypeptides are generally water soluble and therefore must be entrapped in the internal water phase of a water/oil/water emulsion. This method ensures polypeptide entrapment within the PLGA microspheres following solvent evaporation. During entrapment of VEGF, addition of phosphatidyl choline (PC) as a surfactant and reduction in the temperature of preparation to 30°C results in improved emulsion stability and hence VEGF content and activity following entrapment in the microspheres. Sucralfate, or other protease inhibitors, may be added to preserve polypeptide activity *in vivo*. Rat serum albumin may also be added to facilitate release rates.

A preferred tissue/implant interface is a hydrogel in which a tissue response modifier is present as part of a microsphere. A preferred amount of tissue response modifier-containing microspheres is 0.1 to 50% (w/v), preferably 1 to 25% (w/v) and more preferably 5 to 10% (w/v) of the hydrogel.

In another embodiment, a mixture of microspheres having different release rates is used to optimize treatment at the site of implantation. For example, it is known that PLGA microspheres often do not release the entrapped drug for 7 to 14 days. This delay reflects the time during which the hydrolytic processes begin the degradation and consequent pore formation and fragmentation of the microspheres, thus enhancing drug egress. The release kinetics and length of this delay may be governed by factors such as microsphere particle size and surface morphology; polymer physicochemistry (e.g. molecular weight, copolymer ratio and crystallinity); as well as the physicochemical properties of the drug. Use of a mixture of microspheres having differential release rates allows tailoring of drug delivery. It is especially useful to tailor continuous and long lasting delivery of anti-inflammatory factors to an implantation site.

While a number of methods of adjusting the release rates of microspheres are known, many require additional steps, thereby increasing cost and chance for contamination. A particularly advantageous method is to "pre-degrade" microspheres, that is, to treat the microsphere and drug so as to result in faster degradation than an untreated microsphere. An exemplary predegradation treatment is by stirring a microsphere in a solvent for a time effective to increase the degradation rate of the microsphere (e.g. stirring in polyvinyl alcohol for 1-2 weeks). Such predegradation can be evidenced by a rough surface of the microsphere as observed by EM techniques.

Conversely, microspheres can also be treated to decrease the rate of degradation, i.e., by treating the microspheres and drug with polyethylene glycol (PEG). PEG treatment of microspheres can delay the start of the linear release period.

A preferred microsphere preparation is a preparation comprising a mixture of untreated and predegraded microspheres. Use of predegraded microspheres minimizes or eliminates the delay time in drug release that prevents the continuous availability of the tissue response modifier up through and possibly beyond the crucial first two weeks after implantation.

In another embodiment, a mixture of PEG-treated microspheres and untreated microspheres is used to provide longer release of the tissue response modifier. Alternatively, adding PEG-treated microspheres to a mixture of predegraded and untreated microspheres

can be used to extend the continuous release of tissue response modifier beyond one month. Thus a combination of predegraded, untreated, and PEG-treated microspheres can provide a continuous release of tissue response modifier upon implantation (without a delay period), through one or more months, or even beyond.

5 In addition to the above-described methods, general methods for the manufacture of the present tissue/implant interfaces will depend on the nature of the implant, the nature of the one more bioactive polymer layers, and the nature of the tissue response modifiers. The part of the implant to be coated may be cast or coated with, or dipped or immersed into a solution of monomer, followed by polymerization onto the implant. Alternatively, the
10 implant may be coated by melting, dipping, casting, or coating with the polymerized monomer, followed by removal of a solvent (if present). Self-assembly type polymer coatings are generally assembled directly on the surface of the implant. The monomer or polymer solutions may comprise the tissue response modifier; thereby incorporating the modifier during deposition, or the tissue response modifier may be adsorbed into the layer
15 after deposition. The amount of tissue response modifier incorporated in the tissue response modifier-delivery device will vary depending on the particular tissue response modifier used, the desired therapeutic effect, and the time-span over which tissue response modifier delivery is desired. Since a variety of devices in a variety of sizes and shapes may be fashioned for control of a variety of tissue responses, the upper and lower limits will depend on the activity
20 of the tissue response modifier(s) and the time span of release from the device desired in a particular application. Thus, it is not practical to define a range for the therapeutically effective amount of the tissue response modifier to include. While the bioactive polymer may assume almost any geometry, layers are generally preferred, being in the range from about 0.05 to about 5 mm thick, preferably from about 0.1 to about 1 mm thick.

25 Determination of the precise tissue/implant configuration and the quantity and form of tissue response modifier effective to control the tissue response at the site of implantation is within the abilities of one of ordinary skill in the art, and will depend on the particular site of implantation, the length of time that the implant is intended to remain in the body, and the implant itself. Exemplary implantation sites include, but are not limited to, parts of various
30 systems such as the gastrointestinal tract, including the biliary tract, urinary tract, genital

tract, central nervous system and endocrine system, and sites such as blood vessels, bones and joints, tendons, nerves, muscles, the head and neck, and organs such as the heart, lungs, skin, liver, pancreas, eye, blood, blood progenitors and bone marrow.

Exemplary implants include, but are not limited to, prostheses, such as joint
5 replacements, artificial tendons and ligaments, dental implants, blood vessel prostheses, heart valves, cochlear replacements, intraocular lens, mammary prostheses, penile and testicular prostheses, and tracheal, laryngeal, and esophageal replacement devices; artificial organs such as heart, liver, pancreas, kidney, and parathyroid; and repair materials and devices such as bone cements, bone defect repairs, bone plates for fracture fixation, heart valves, catheters,
10 nerve regeneration channels, corneal bandages, skin repair templates, and scaffolds for tissue repair and regeneration; and devices such as pacemakers, implantable drug delivery systems (e.g., for drugs, human growth hormone, insulin, bone growth factors, and other hormones), and biosensors. Implantable drug delivery systems are disclosed in U.S. Patent No. 3,773,919, No. 4,155,992, No. 4,379,138, No. 4,130,639, No. 4,900,556, No. 4,186,189, No.
15 5,593,697, and No. 5,342,622, which are incorporated by reference herein. Biosensors for monitoring conditions such as blood pH, ion concentration, metabolite levels, clinical chemistry analyses, oxygen concentration, carbon dioxide concentration, pressure, and glucose levels are known. Blood glucose levels, for example, may be monitored using optical sensors and electrochemical sensors. Various UV, HPLC and protein activity assays
20 are known or can be modified to provide quantitation of the release rates, concentration, and activity of the tissue response modifiers *in vitro* and *in vivo*.

The above-described embodiments alone or in various combinations are all within the scope of the present invention. A schematic diagram of an exemplary tissue/implant interface 10 comprising an implant 12 and a hydrogel 14 is shown in FIG. 1. Tissue response
25 modifiers 16 are entrapped within hydrogel 14, while tissue response modifiers 18 are covalently attached within hydrogel 14. The covalent attachments may be permanent, or hydrolysable. Tissue response modifiers 19 are associated with the surface of hydrogel 14, e.g., by ionic, hydrophilic, or hydrophobic interactions. Tissue response modifiers 20 are contained within microspheres 22, which are entrapped within hydrogel 14; tissue response
30 modifiers 24 are contained within microspheres 26, which are covalently attached to hydrogel

14; and tissue response modifiers 28 are contained within microspheres 30, which are associated (by ionic or hydrophobic interactions, e.g.) with hydrogel 14. Tissue response modifiers 32 are contained within nanoparticles 34, which are entrapped within hydrogel 14. PEO chains 40 and PC chains 42 are covalently attached to the exterior surface of hydrogel 14. Adhesive ligands 44 are covalently attached to a plurality of PEO chains 40. In a further embodiment, one or more membrane layers may be disposed between implant 12 and hydrogel 14 (not shown). The membrane layers may advantageously be semi-permeable, allowing the diffusion of selected molecules to the implant surface. Inclusion of other bioactive agents in the tissue/implant interface having local or systemic effects (e.g., antibiotics, sedatives, hormones, anti-infectives, anti-fungals, analgesics, DNA, RNA, and the like) is also within the scope of the present invention.

A schematic diagram of an exemplary tissue/implant interface 100 comprising an implant 110, a mussel adhesive protein layer 112, and an alternating polycation/polyanion film 114 is shown in FIG. 2. Polycation/polyanion film 114 comprises tissue response modifiers 116 encapsulated by microspheres 118, which are entrapped within film 114. Tissue response modifiers 120 (e.g., VEGF) and adhesion ligands 122 are present external to polycation/polyanion film 114. PEO may be added to the assembly to control protein adhesion (not shown).

An exemplary application of the present invention is a stent used to keep the blood vessel open following balloon angioplasty, wherein at least a part of the outer surface of the stent comprises a bioactive polymer layer comprising microsphere-encapsulated drugs, e.g., Dexamethasone, to prevent the inflammatory response and excess tissue regeneration (restinosis). Such microspheres administered intravenously would be washed away by the rapid flow of blood.

Another exemplary application of the above-described tissue/implant interface comprises an implantable electrochemical blood glucose sensor. Preferably, the electrochemical sensor monitors glucose concentration in subcutaneous tissue, using hydrogen peroxide-based amperometric detection. These sensors are highly specific for glucose, have a short response time, and may be readily miniaturized. As shown in FIG. 3, a preferred sensor 330 has a glucose-indicating (working) electrode 332 (the glucose-indicating

electrode), and a reference-counter electrode 336. Working electrode 332 may comprise a coiled platinum wire 334, and reference electrode 336 may comprise a coiled silver/silver chloride wire 337. Glucose oxidase is immobilized in a matrix 338, for example bovine serum albumin/glutaraldehyde. In the presence of oxygen, glucose is oxidized by the enzyme, producing hydrogen peroxide (H_2O_2). The hydrogen peroxide is then oxidized at the surface of working electrode 334, thereby producing a measurable electric current, wherein the amount of current is proportional to the quantity of glucose present at the electrode. Sensor 330 has a linear response from zero to at least 20 millimolar (mM) glucose in vitro, with high sensitivity. Sensor 330 is about 0.5 mm in diameter, but may be made larger or smaller as the application dictates.

As shown in detail in FIG. 4, at least a portion of sensor 330 is protected from interaction with the surrounding tissue by the presence of a selectively permeable membrane. Platinum wire 334, for example, is coated with at least one selectively permeable membrane 320 for preventing or minimizing tissue interactions. An exemplary selectively permeable membrane is an electrodeposited poly(o-phenyldiamine) (PPD) film, which is permeable to hydrogen peroxide, but is impermeable to larger, interfering and/or degradative molecules such as ascorbic acid, uric acid, proteins, and the like.

The entire sensor 330 further comprises a first bioactive polymer layer 322, which further protects the sensor from interfering and/or degradative substances present in the tissue, such as proteins. As described above, an exemplary material is a perfluorinated ionomer membrane, e.g., NAFIONTM, which has been suitably modified to prevent calcification and other undesirable interactions. A second bioactive polymer layer 344, e.g., a hydrogel, is directly adjacent layer 322. Tissue response modifiers 350 are covalently bound to semipermeable membrane 320, first layer 322, and second layer 344. Tissue response modifiers 352 are also associated with second layer 344 in slow-release form to provide long-term delivery of the tissue response modifier to the site of implantation. Other glucose sensors are disclosed in U.S. Patent No. 4,703,756, which is incorporated by reference herein.

The invention is further illustrated by the following non-limiting examples.

EXAMPLES

Example 1. Hydrogel Synthesis.

Hydrogels of HEMA, FOSA and NVP (with a variety of monomer ratios) were polymerized using 0.1 mole% AIBN as a free radical initiator in bulk at 70°C and in water/dioxane at 60°C. After 12-24 hours, crosslinked materials were obtained which were insoluble in water, acetone and a variety of other organic solvents. Residual monomer was removed by swelling in water/acetone followed by repeated rinsing. The degree of swelling depended on the relative weight percent (wt. %) of each monomers used to form the gel. The impact of hydrogel composition (wt. % based on total amount of monomers) on swelling was determined and the results are shown in Table 1.

Table 1.

Sample No.	HEMA	NVP	FOSA	PEG-Acrylate	Swelling*
1	100	0	0	0	73
2	94	0	6	0	64
3	62	32	6	0	97
4	35	59	6	0	244
5	56	28	6	10	110
6	40	24	6	30	140

*average percent increase in weight after 14 hours in distilled H₂O at 37°C

These data indicate that only 5% incorporated FOSA monomer can decrease the swelling in distilled H₂O by 10%. The addition of NVP monomer can increase the swelling to various amounts based on the charge ratio of the monomer. The incorporation of the PEG acrylate monomer can also effect the swelling properties while potentially decreasing protein adsorption. Data indicate that the proposed materials can be successfully prepared with as many as four co-monomers, and that they exhibit appropriate hydrogel properties that can be well controlled. These hydrogels also contain residual hydroxyl functionality that may be employed to covalently attach tissue response modifiers and/or slow release delivery systems using known procedures

Example 2. Preparation of HEMA-FOSA Hydrogels

To prepare this gel, 2.45 g of HEMA (Aldrich, used as received), 15 g of FOSA ("AFX-13" from 3M, recrystallized 3 times in methanol), 0.007 g AIBN (Aldrich, recrystallized in methanol) were mixed with the aid of 1.5 mL dioxane (Aldrich, used as received). This solution was poured into a Teflon mold which was then placed in an oven at 70°C for 12 hours. The gel was then swollen in water and water/acetone mixtures to leach out unreacted monomer and linear (uncrosslinked) polymer. The resultant gel swollen to equilibrium in deionized water had a thickness of 1mm. For permeability measurements, a circle of appropriate size (1.5 cm diameter) was stamped out of the gel.

Example 3. Determination of Permeability of HEMA-FOSA Hydrogels *In Vitro*.

To determine permeability of the new HEMA-FOSA hydrogels to glucose, the free-standing hydrogel film was supported by a 1.5 cm diameter polycarbonate membrane having 10-micron sized pores. The permeability of the HEMA-FOSA hydrogel to glucose is determined using a single-sided magnetic biodialyser (Sialomed Corp.). This device consists of a sample chamber having an opening which is covered with the supported HEMA-FOSA hydrogel. When the chamber top is screwed on, it secures the membranes in place, but does not cover the membranes. This entire apparatus is placed into a beaker containing the dialysis buffer, and stirred at a fixed rate and temperature (37°C). Over time, the content of the sample chamber diffuses into the buffer. The interior of the chamber is filled with 1 mL of 1M glucose in phosphate buffer solution (PBS), in PBS with physiologically relevant proteins (albumin, complement, fibrinogen, fibrin, and fibronectin), in cell culture medium, and in cell culture medium with cells (vascular endothelial cells and fibroblasts). The dialysis buffer (B) consists of 50 mL of the same solution, but without glucose. This high sample to buffer ratio ensures that the change in glucose concentration in the dialysis buffer over time is measurable. Samples (50 micro liters) of the dialysis buffer are collected at 20 minute intervals for 2 hours. The concentration of glucose in the dialysis buffer samples is quantified using a Beckman Glucose Analyzer II. Using this protocol, the permeability of the polycarbonate membrane (for reference), NAFION and HEMA-FOSA hydrogel is assessed, as shown in FIG. 5. Based on these data, use of the hydrogels should only slightly reduce the permeability to glucose because of the high water content of the materials.

Example 4. Preparation of VEGF-Poly(HEMA).

VEGF was incorporated into hydrogels comprising poly(HEMA) and sucralfate (a protease inhibitor) by incubating the hydrogel with 0.075 microgram/microliter of VEGF. The samples were then allowed to air dry for about 2 hours at room temperature.

5 An ELISA assay (R&D Systems, Minneapolis, MD) is used to quantify VEGF during bioactive layer or slow release delivery system preparation. To conserve VEGF (or other valuable tissue response modifier), release studies are conducted using a miniaturized, high throughput method, wherein tissue response modifier-microsphere samples are placed in 12 well plates with phosphate buffer (pH 7.4, 37°C) and volumes are adjusted to maintain sink
10 conditions. At appropriate time points, samples are removed and analyzed for tissue response modifier content. In addition, the *in vitro* release studies are conducted in the presence of 1) protein and 2) cells (leucocytes, vascular endothelial cells and fibroblasts) in attempt to mimic the *in vivo* environment at the implant/tissue interphase. VEGF activity is monitored by a cell proliferation assay *in vitro* as described by J. U. Muhlhauser et al., in Circulation
15 Research, Vol. 77, p. 1077 (1995) and radioactivity monitoring using ¹²⁵I-VEGF (new England Nuclear, Boston, MA) *in vivo*. Ultraviolet (UV) analysis and high pressure liquid chromatography (HPLC) assays are available to quantify dexamethasone concentrations *in vitro* and *in vivo*, respectively. Partition coefficient data may also be used to determine tissue response modifier distribution during preparation.

20 Example 5. VEGF-Induced Neovascularization in Rats.

A simple hydrogel model of local drug delivery was used to demonstrate that the presence of VEGF at the implant/tissue interface will induce neovascularization in rats. Accordingly, the above-described VEGF-poly(HEMA) with sucralfate was subcutaneously
25 implanted in Sprague-Dawley rats. To control for non-specific effects, hydrogels comprising poly(HEMA) and sucralfate (with no VEGF) were also implanted into Sprague-Dawley rats. Two weeks after implantation, the animals were sacrificed and the implantation sites were examined for neovascularization. An implant comprising poly(HEMA) and sucralfate, but without VEGF failed to induce any detectable vascularization. In contrast, implantation of
30 the hydrogel comprising poly(HEMA), sucralfate, and VEGF induced massive

neovascularization in the rat subcutaneous tissue. These data clearly demonstrate that use of angiogenic factors enhances the vasculature around an implant.

Example 6. Preparation and Characterization of NAFIONJ-Fe³⁺ Self-Assemblies.

5 NAFIONTM, a perfluorinated ion-exchange resin (5% w/v in lower aliphatic alcohol mixture and water; equivalent weight of 1100 g of polymer per mol of -SO₃H) and hexahydroferric chloride (FeCl₃·6H₂O) and ferric citrate were obtained from Aldrich. A.C.S. certified KCl was purchased from Fischer and used without further purification. 28-30 wt. % aqueous solution of NH₄OH (Acros) and 35-38% hydrochloric acid (J.T. Baker) were used
10 as a 1% dilution to adjust pH. Millipore quality deionized water was utilized in all experiments.

Silicon wafers with native oxide (100 orientation) and microscope glass slides (Fisher) were used as substrates for the self-assembly. These were cleaned in pirahana solution (H₂SO₄/H₂O₂ (7:3)), rinsed with deionized water and methanol, kept in deionized
15 water overnight and used for the self-assembly growth without further surface modification. 1 mg/mL (9.09 x 10⁻⁴M), based on the repeat unit molecular weight) NAFIONTM solution was prepared by diluting the as received solution in a (9:1) methanol / water mixture and used for all experiments. The pH of these solutions was adjusted with aqueous NH₄OH solution. In addition, the ionic strength of NAFIONTM solutions was modified with KCl. 0.5 g of
20 FeCl₃·6H₂O was solubilized in 100 mL of water to produce a 5 mg/mL (18.5 x 10⁻³ M) solution. Similar ferric citrate solutions were also prepared, where the pH of these solution could be varied from 2 - 6 with slow addition of base. This greatly minimizes Fe³⁺ afflicted damage to the glucose oxidase enzyme.

An HMSTM Series Programmable Slide Stainer (Carl Zeiss, Inc.) was used for the
25 layer-by-layer assembly of NAFIONTM with Fe³⁺. The sample holder in the HMSTM Series Slide Stainer was covered to reduce solvent evaporation particularly obvious around the substrate edges, thereby improving film quality. Each dip cycle consist of 8 steps. First the substrates were immersed in NAFIONTM solution for 15 minutes followed by 3 consecutive washing step, of one minute each in Millipore quality deionized water. Subsequently, the
30 substrates were dipped into ferric chloride solution for 15 minutes followed by three washes

as before. 12 subsequent dip-cycles were usually employed in this study. The substrates were constantly agitated throughout the dip-cycle to improve film quality. After completion of a desired number of dip cycles the substrates were removed and rinsed with Millipore water and methanol and dried with air.

5 Solubility studies in a series of solvents have led to the conclusion that depending on the dielectric constant of the solvent or solvent mixture, NAFION™ forms either homogeneous mixtures, colloids or precipitates. Based on a 9/1 methanol/water solvent ratio used in this study (ϵ approximately 38), NAFION™ is expected to attain a micellar conformation with the hydrophobic fluorocarbon backbone buried inside and the polar
10 sulfonate groups located on the surface.

FIG. 6 illustrates the ellipsometrically determined film thickness as a function of number of dip cycles. Maintaining the pH of FeCl₃ and wash solutions constant, the pH of NAFION™ solution was found to have a profound influence in film growth. The fastest growth rate was observed at pH 3, corresponding to c.a. 40 nm per dip cycle. A abrupt
15 transition in film growth is observed above pH of 4, leading to significantly lower deposition rates (i.e. 6.7 and 6.3 nm/dip-cycle for pH of 4.5 and 5.5 respectively).

Table 2 illustrates the hydrodynamic radius R_H and diffusion coefficient D_H of NAFION™ solutions as determined by dynamic light scattering (DLS).

20 Table 2.

pH	NAFIONJ With 0.01 KCl		NAFIONJ Without KCl	
	R_H (nm)	D (cm ² s ⁻¹)	R_H (nm)	D (cm ² s ⁻¹)
5.5	51.0	8.5×10^{-8}	115.9	3.75×10^{-8}
3.0	45.8	9.5×10^{-8}	113.5	3.83×10^{-8}

The influence of pH on the hydrodynamic radius of NAFION™ appears to be negligible for pH of 3 and 5.5. This concurs with the strong acidic character of sulfonate groups (NAFION's™ acidity -H₂ of about 12 in terms of Hammett acidity is comparable with 100%
25 sulfuric acid) implying a nearly complete degree of ionization for both pH 3 and pH 5.5. On

the other hand, the tendency of ferric ions to form insoluble hydroxides starts around pH greater than or equal to 4.3 based on solubility product of $\text{Fe}(\text{OH})_3$ (K_{sp} about 6×10^{-39}). This transformation of absorbed Fe^{3+} to $\text{Fe}(\text{RSO}_3)_x(\text{OH})_{1-x}$ results in increasing the basicity of the substrate. Based on these observations, the abrupt transition to lower growth rate of the NAFIONTM/Fe³⁺ assemblies could be associated with neutralization-induced NAFIONTM spreading.

FIG. 7 depicts film thickness of these assemblies as a function of the pH and ionic strength of NAFIONTM solution. The addition of 0.01 M KCl was found to have a profound effect in the film growth rate. The influence of salt concentration on the thickness of the deposited films was also investigated, with the above value determined as optimum ionic strength based on film quality. At higher KCl concentrations i.e., 0.1 M, no film deposition was observed and salt was preferentially precipitating on the surface.

The well documented charge screening effect in polyelectrolytes, as a result of diminishing repulsive interactions between the negatively charged sulfonate groups, by addition of positively charged ions (i.e., K^+), allows NAFIONTM to attain a more compact conformation. This results in nearly 60% reduction in hydrodynamic volume as compared to salt-free solutions (see Table 2). The comparable increase in diffusion coefficient of NAFIONTM micelles imply greater diffusion rate on the assembly surface. Surprisingly enough, the average growth rate shown in Figure 2A (pH 3, 0.01 M KCl), which is c.a. 47 nm/dip-cycle, corresponds roughly to the hydrodynamic radius shown in Table 1. This implies that surface adsorption is accompanied with minimum NAFIONTM surface-spreading, relative to the no-salt case, where a nearly 65% spreading results in 40 nm/dip-cycle growth rate. The effect of salt appears to be equivalent for different pHs based on the relative strength of the surface-induced interactions that tend to flatten the micelle and charge-screening forces that try to keep it intact. It appears that at pH of 3, the latter is the dominant effect, with the case inversed for pH of 4.5, where the basicity of $\text{Fe}(\text{RSO}_3)_x(\text{OH})_{1-x}$ overpower the charge-screening forces. This thermodynamic based model could, however be subject to certain kinetic imposed restrictions with respect to the rate of micelle arrival to the surface, as inferred by the larger diffusion coefficients in the presence of salt. EDAX of self-assembled NAFIONTM/Fe₃₊ films, treated in DMEM nutrient mixture showed more than two

orders of magnitude decrease in intensity of calcium line compared to NAFION™ films deposited by dip-coating.

FIG. 8 illustrates the glucose permeability data obtained with these assemblies on 0.1 micron glass fiber membranes.

5

Example 7. Preparation and Characterization of Humic Acid Self-Assemblies.

Humic acid solutions were prepared (1 mg/mL concentration) by dissolving 1 g of humic acid (HA, used as obtained), sodium salt (obtained by Aldrich) in 1 L of deionized water. The pH of the resulting solution was found to be 9.3. The pH of the HA solution can
10 be varied by addition of acid (e.g., HCl), thus greatly modifying the degree of ionization of carboxylic groups in HA and significantly affecting the molecular conformation of the polymer in solution. The resulting net thickness of the deposited film increases with decreasing pH due to the natural coiling up of the polyionic molecules as its degree of ionization decreases. A very similar effect is observed in the presence of salt. Salt induced
15 charge screening effects allows attaining more compact coiled conformations at the same pH and thus consequently thicker films are formed. Quartz Crystal Microbalance (QCM) (FIG. 4) and ellipsometric data (FIG. 10) support these observations.

Example 8. *In Vitro* Response to a Glucose Sensor Comprising a Bioactive Layer 20 (Prospective).

The function of the glucose sensor comprising a bioactive layer alone is assessed by incubating the sensors at 37°C in PBS with and without physiologically relevant proteins (albumin, complement, fibrinogen, fibrin, and fibronectin, and the like), and in culture media with or without physiologically relevant cells (cells vascular endothelial cells, fibroblasts, and
25 the like). All test buffers and culture media contain 5.6 mM glucose. The sensors are continuously polarized at ± 0.7 V. To test the sensors, increasing amounts of a sterile glucose is added, and the sensitivity (in nA/mM), the background current, and the response time of the sensors is determined. The effect of compounds such as ascorbic acid, uric acid, and acetaminophen, which are known to interfere with the response of glucose sensors, is also

evaluated to select the sensor configuration that offers the best protection against electrochemical interferences.

Example 9. *In Vitro* Response to a Glucose Sensor Comprising a Bioactive Layer and Tissue Response Modifier(s) (Prospective).

Adsorption of key plasma and tissue proteins onto the implant surfaces and/or bioactive layers is evaluated using radioactive labeled proteins, for example albumin, the third component of Complement (C3) and fibrinogen/fibrin, and fibronectin. Once the general binding characteristics of these proteins are established, the ability of the same materials to activate the complement and coagulation pathways present in plasma is determined.

Determining *in vitro* which implant/bioactive layer/tissue response modifier configurations minimize fibroblast migration, proliferation and collagen synthesis, and maximize vascular endothelial cell proliferation and migration allows design of implant configurations that will be optimal in extending implant lifetime *in vivo*. Impact on fibroblast and vascular endothelial cell proliferation is quantified using the standard H^3 Thymidine assay. Fibroblast synthesis of collagens (type III and type I) are quantified using hydroxyproline incorporation and ELISA assays. Fibroblast and vascular endothelial cell migration are determined using computer aided video microscopy and the microcarrier bead assay.

Example 10. *In Vivo* Tissue Response to of a Glucose Sensor (Control).

To characterize baseline tissue reactions, a glucose sensor without tissue response modifiers was constructed as shown in FIG. 1 at 10, comprising glucose-indicating (working) electrode 12 and a reference-counter electrode 16. Glucose oxidase was immobilized in a bovine serum albumin/glutaraldehyde matrix 18. Sensor 10 further comprised an outer membrane of NAFION, which is thermally conditioned at 120° or above to prevent *in vivo* degradation. The thermally annealed sensor showed a linear response up to at least 20 mM glucose and a slope of 3.2 nA/mM with an intercept of 5.7 nA. The response time of the sensor was about 30 seconds and the time required for the background current to decay to

steady state after initial polarization was about 35 min. The sensor had a high selectivity for glucose, and a low partial pressure of O₂ affected the response of the sensor only for levels below 8 mm Hg.

The sensors were implanted in the back of dogs and were tested regularly over a 10 day period. About 45 minutes was required for the current to stabilize after polarization *in vivo*. After this period a bolus intravenous injection of glucose was made and the sensor output was monitored. Blood was periodically sampled from an indwelling catheter to determine blood glucose levels. A 5-10 minute delay was observed between the maxima in blood glucose and the sensor's signal, corresponding to the known lag time between blood and subcutaneous glucose levels. Although experiments with dogs showed that the response of some of the sensors remained stable for at least 10 days, others failed. This lack of reliability, which is common to all implantable glucose sensors developed worldwide, is believed to be mostly caused by the tissue reaction to the sensor.

In addition, the sensors were implanted in Sprague-Dawley rats and tissue samples removed one day and one month after implantation. The specimens were processed for traditional histopathology using H&E staining, as well as trichrome staining (fibrin and collagen deposition). At one-day post-implantation, a massive inflammatory reaction was observed at the tissue site around the sensor. The inflammatory reaction comprised primarily polymorphonuclear (PMN) and mononuclear leukocytes, as well as fibrin deposition. By one-month post-implantation, significant chronic inflammation and fibrosis were present at the tissue site around the sensor, together with mature collagen and fibroblasts, and loss of vasculature. The chronic inflammation seen at one month appeared to be lymphocytic in nature.

Example 11. *In Vivo* Response to Implantation of a Glucose Sensor Comprising a Bioactive Layer and Tissue Response Modifier(s) (Prospective)

Diabetes is induced in rats by intraperitoneal (I.P.) injection of streptozotocin (75 mg/kg) 10 days before an implantation, and monitored using test strips. Animals are also monitored daily for clinical symptoms of distress, and animals showing significant clinical distress are sacrificed. Sensors comprising a semipermeable membrane and a bioactive layer

are implanted into the interscapular subcutaneous tissue of anesthetized normal and diabetic rats (250-300 g body weight). Two sensors per rat are implanted. To minimize tissue damage, the sensors are implanted through a thin wall needle (18 to 20 Gauge), and the needle is removed, leaving the sensor in place with the connecting leads exiting the skin. The leads are secured to the skin to prevent removal of the sensor.

Response of the sensors is tested on days 0, 3, 7, 14, 21, and 28. During each test, the rats are anesthetized, and then prior to administering glucose, the sensors are connected to a small potentiostat (Petit Ampere, BAS) and subjected to 0.7 V. The current produced by the sensor is either read directly on the digital display of the potentiostat or recorded on a small strip-chart recorder. After a "run-in-period" of about 1 hour to obtain a stable signal, a glucose solution (30% solution, 1.0 g/kg body weight) is injected intraperitoneally (I.P.). Plasma glucose concentration is determined in blood samples obtained from the tail vein using a heparinized Pasteur pipette. The concentration of glucose in the blood samples is measured using a Beckman Glucose Analyzer II. The glycemia of the rat is correlated with the current produced by the sensor. *In vivo* studies have demonstrated that plasma glucose increases to a plateau that lasts at least 10 minutes. This time interval is long enough to establish equilibration between the plasma and subcutaneous glucose concentrations. By using the plasma glucose values and the corresponding current levels at both the basal state and the peak, an *in vivo* sensitivity coefficient (in nA/mM) and the extrapolated background current is determined.

To better assess the response time of the sensor, an Intravenous Glucose Tolerance Test (IVGTT) is performed on some animals. For this test, before sacrificing the animal at the end of each 4 week study, a catheter is placed in a jugular vein of the anesthetized rat, and glucose is rapidly injected intravenously (I.V.). The I.V. injection of glucose will allow for a better determination of the response time of the sensor since the change in glucose levels will be more rapid than the I.P. injection of glucose. The glycemia of the rat and the current produced by the sensor will be measured and correlated as above.

Additionally, tissue response modifier *in vivo* partitioning affects the pharmacokinetic (PK) data. Intravenous and sub-cutaneous solution PK data in normal and treated animal models (e.g., rats) are used to calculate local effective concentrations to

control inflammation, fibrosis and neovascularization, and as a starting point to calculate microsphere drug loading and release rates. Solution PK data are necessary in deconvolution (mathematical separation) of microsphere PK data, as tissue response modifier PK often alters in the microspheres.

5 Accordingly, the subject implant and its associated hydrogel is implanted in normal and treated animals. A deconvolution, model-independent approach and the Wagner-Nelson method is used to analyze the plasma concentration time profiles. The response of normal animals to a subcutaneous implantation comprising a hydrogel and associated tissue response modifiers is investigated using standard histologic-based protocols.

10 Sensors that lose their function *in vivo* are explanted and the surrounding tissue removed. To determine the cause for failure, the explanted sensors are re-tested *in vitro* to evaluate their *in vitro* response. Some sensors are also used for surface analysis to determine chemical and physical changes of the sensor membranes and interactive hydrogels.

15 Example 12. Formation of Standard and Degraded Microspheres

PLGA microspheres loaded with dexamethasone were prepared by an oil-in-water (o/w) emulsion/solvent evaporation technique. The oil phase consisted of 20 mg of dexamethasone added to 5 ml of a mixture of 9:1 dichloromethane to methanol in which was dissolved 100 mg of PLGA (average molecular weight 40,000 to 70,000) (2% w/v). The
20 dexamethasone and PLGA were used as received from Sigma. This oil phase was added to 100 ml of 0.2% (w/v) PVA solution, which was stirred at 1250 RPM for 30 minutes to achieve emulsification and the desired droplet size range. The resulting emulsion was stirred on a magnetic stir plate for approximately 16 hours to allow complete solvent evaporation. Alternative formulations were made with the addition of polyethylene glycol of 8,000 (or
25 3,350) molecular weight to the (2% w/v) oil phase. Ten percent of the PLGA dissolved in the mixture of 9:1 dichloromethane to methanol was replaced by PEG.

Predegradation of the microspheres was achieved by stirring for one or two weeks in the PVA solution.

The resulting microspheres were collected from the PVA solution by centrifugation at 8,000 RPM (6,500 g). The microspheres were washed twice with distilled, deionized water, and lyophilized to dry, remove any trace of solvents, and extend the storage life.

Each microsphere system was examined at 200x, 400x, and 600x magnification using a Nikon microscope with a digital camera attached. The morphology of the microspheres was examined as well as the presence of any non-encapsulated dexamethasone. Samples of predegraded and non-predegraded microspheres were placed on top of carbon tape, and covered with 20 nm of gold using a sputter coater following a standard procedure for scanning electron microscopy (SEM) studies. These samples were examined at 150x to 3000x magnification in an JEOL JSM-6320F SEM.

The microspheres had a regular spherical morphology as shown in Figure 11. The surfaces of the two types differ, as can be seen at high magnification (A and C). The surface of the standard microspheres (A and E) was smooth, while the surface of the predegraded microspheres (B and D) had surface irregularities. The irregularities in the surface of the microspheres are caused by the degradation of the PLGA. The irregularities range from dimples reflecting a channel into the PLGA, to entire regions with a rough irregular degraded surface. In the low magnification images (C and D), the surface topography is not visible, but a representative distribution of the microsphere sizes for both standard and predegraded microspheres are shown. The microspheres had a Gaussian distribution of particle sizes ranging from 1 to 50 μm in diameter. Approximately 100,000 particles were counted for each sample. The average diameter size was 11 plus or minus 1 μm for the standard microspheres and 12 plus or minus 2 μm for predegraded microspheres. Predegrading microspheres caused no significance change in particle size.

An excess of dexamethasone was used in formulating the microspheres in order to maximize the amount encapsulated. Theoretically 16% encapsulation was possible, but not realistically expected. The encapsulation percentage for the microspheres was low, approximately 4% once any free dexamethasone was removed. The encapsulation percentage of the predegraded microspheres was further lowered by approximately the amount of the burst release. The PEG formulation of the microspheres had approximately 3% encapsulation.

Example 13: Dexamethasone Degradation

The degradation of dexamethasone was studied in PBS at 37°C. For this study, three 25-30 ml aliquots of a dexamethasone calibration standard in PBS with and without sodium azide were placed in amber vials in the same constant temperature warm room (37°C) as used for the *in vitro* release studies. The aliquots without azide were kept in sealed containers and opened aseptically, as necessary, in a laminar flow hood. Every few days, 0.5 ml was removed from each aliquot by syringe. These samples were analyzed using a Varian high performance liquid chromatography (HPLC) consisting of a model 345 dual wavelength UV detector, a Prostar 210 solvent delivery system with an in line filter and degasser and Dynamax HPLC Method Manager analytical software. Analysis was performed at 246 nm using a Waters 290 mm reversed phase μ Bondapak C-18 column with a mobile phase of 40% 2 mM acetate buffer (pH 4.8) and 60% acetonitrile flowing at 1 ml/min. All data points for each of three samples at each time point were included in the graph to determine the degradation rate.

Degradation of dexamethasone has been correlated with the formation of a secondary HPLC peak that is a dexamethasone degradation product. The degradation of dexamethasone may be due to microbiological action or environmental factors such as temperature, exposure to PBS (water), or pH. The pH of the PBS in the release studies was checked after 2 months had elapsed and was still within the range of 7.0 to 7.4. Therefore, the volume of PBS necessary to maintain sink conditions and its buffering capacity was sufficient to diminish any effects of the PLGA degradation on bulk solution pH. However, this did not eliminate the possibility that lowered pH inside the microspheres may contribute to dexamethasone degradation. Previous *in vitro* studies have shown that PLGA degradation causes a decrease in pH in the interior of the microspheres. Therefore, to eliminate the possibility of degradation by low pH, degradation studies were performed on dexamethasone (without PLGA) in PBS solution at pH 7.4. A decrease in dexamethasone concentration was still observed despite the constant pH of 7.4. This ruled out pH as being the cause of degradation of dexamethasone in the microsphere release studies. Dexamethasone standards prepared in PBS with and without sodium azide were used to comparatively study drug degradation by microbiological action at elevated temperatures. Aliquots of these dexamethasone standards were placed in the same constant temperature (37°C) warm room as used for the *in vitro* release studies. The dexamethasone concentrations in all

cases decreased steadily as shown in Figure 12, with and without sodium azide. Therefore, degradation was not due to microbiological action.

A plot of the loss of concentration of dexamethasone versus the area of the new secondary peak (standardized for the injection volume) resulted in a linear relationship (see Figure 13), inferring that the loss of dexamethasone in the *in vitro* release studies was a consequence of the production of this degradation product. Linear regression of this data provided a function to correlate the secondary peak to the amount of dexamethasone degraded. This function as well as the correlation constant is provided in Figure 13. The function shown in Figure 13 was subsequently used to correct the *in vitro* release study results to account for dexamethasone degradation. Previous studies have shown the importance of drug stability on the analysis of release data from controlled release microspheres, and a model was developed to account for drug degradation.

Example 14: Release of Dexamethasone from Standard Microspheres

The *in vitro* release study was performed in phosphate buffered saline (PBS) with 0.01% (w/v) sodium azide under sink conditions. The *in vitro* release studies were performed on a stir plate in a constant temperature (37°C) warm room. Five to 10 mg samples of microspheres were added to 100 ml of PBS in sealed amber jars. At set time intervals, 2 ml samples were taken for analysis by syringe through a sterile 0.22 μ m filter. The microspheres pulled into the syringe filter were returned by "back washing" 2 ml of replacement PBS through the syringe filter into the jars. Analyses of the release samples were performed using HPLC, as described above, with a mobile phase of 50:50 2 mM acetate buffer (pH 4.8) to acetonitrile flowing at 1 ml/min. Three batches of microspheres were investigated and the means and standard deviations reported.

Figure 14 shows that the standard microspheres (without predegradation) had an initial burst release followed by a delay and then continued release of dexamethasone. The initial burst release was due to microsphere surface associated drug. The delay reflected the time necessary for PLGA hydrolysis to erode sufficient PLGA to allow dissolution and release of entrapped drug. In biomedical applications (such as biosensor implants), this delay would prevent availability of drug for inflammation suppression during the crucial first two weeks post implantation. The second period of drug release continued over the one month study period.

Both periods of release, 1 day to 2 weeks and 2 weeks to 1 month, appeared to have linear or zero order release rates. Release rates follow the rate equation below:

$$C=C_0(e^{-kt})$$

C = concentration of released drug, C_0 = the release rate coefficient or the slope of the release plot, k = release constant, t = time.

Example 15: Dexamethasone Release from Mixed Standard and Predegraded Microspheres

A mixed system of predegraded microspheres was developed to provide continuous release of dexamethasone starting immediately after implantation to up to four weeks. This microsphere system was an equal mixture (1:1:1) of microspheres which had been predegraded for one week, two weeks, and not at all. The microspheres were washed twice in isopropanol for a few minutes and collected by filtration (sterile 0.2 μ m filters). After the isopropanol had completely evaporated, the microspheres were washed again with water and collected by filtration to eliminate any excess free drug. *In vitro* release of dexamethasone by this mixed microspheres system was evaluated for over four weeks in PBS at 37°C. The dexamethasone concentration in the release medium (PBS) was measured (using HPLC) at various time points and the means and standard deviations (for n=3) reported.

The predegraded microspheres released dexamethasone continuously with no delay (Figure 15). The initial burst release of dexamethasone was due to the dissolution of dexamethasone in the outer surface of the microspheres. The release rate appeared to have a linear or zero order release rate from days 1 to 12. The release rate decreased as the microspheres became depleted of drug.

The predegraded and standard microspheres were then combined to provide continuous release over one month (Figure 16). One third of the combined batches was predegraded for two weeks, another third for only one week and one third was standard microspheres. All batches were washed with isopropanol to eliminate any free drug crystals.

The release profile of this mixed predegraded microsphere system began with an initial burst release and continued with an approximately zero order rate for one month (Figure 16). The initial burst release was due to diffusion of the dexamethasone on or near the surface of the microspheres.

PEG was added during microsphere preparation to determine if it could extend the microsphere release. The addition of 10% w/w PEG to the PLGA in the oil phase extended the delay in the dexamethasone release from 11 days to 21 days compared to standard microspheres (Figure 17). Mixing these microspheres with the predegraded and standard microspheres could be used to continue zero order release beyond the one month period.

Example 16: Fabrication and Characterization of Hydrogels Comprising Microspheres

PVA hydrogels were fabricated using a freezing/thawing method to physically crosslink the PVA chains excluding water molecules. Dexamethasone loaded poly(lactic-co-glycolic) acid (PLGA) microspheres were prepared using a solid-in-oil-in-water solvent evaporation technique. Either dexamethasone or the dexamethasone loaded microspheres were incorporated into the PVA hydrogel by suspension in the PVA solution (5% w/v) prior to the freezing/thaw cycle. The number of freezing/thaw cycle steps (3-5 cycles) and the presence of various additives (acrylic acid, humic acid and Nafion) were used to control the physico-chemical properties of the hydrogel and consequently the *in vitro* release rate of dexamethasone.

The PVA hydrogel was characterized for swelling capacity and mechanical properties by monitoring weight and dimensional changes, respectively, as a function of immersion time under constant load of 20 mN using a Perkin-Elmer thermo-mechanical analyzer (TMA). *In vitro* release was conducted in pH 7.4 PBS at 37°C and 100 rpm for 30 days. Dexamethasone was analyzed at 246 nm using HPLC equipped with a C18 column (Waters, Nova-Pak, 3.9 x 150 mm) and a 50:50 mixture of 2 mM acetate buffer (pH 4.8) and acetonitrile as the solvent system.

Example 17: Release of Dexamethasone from PVA Hydrogels

Release of dexamethasone alone from the hydrogels was dependent on the number of freezing/thaw cycles, with release rates decreasing with increase in the number of cycles (approximately 80 – 100 % of dexamethasone was released within 15 days, depending on the number of cycles) (Figure 18). Thus, increasing the amount of crosslinking in a PVA gel decreases the release of an embedded agent such as dexamethasone.

Example 18: Release of Dexamethasone from Microspheres Embedded in PVA Hydrogels

Release rates from incorporated microspheres were much slower with less than 5% released in 30 days. It is hypothesized that the slow release is a result of the buffer capacity of PVA preventing the degradation of the PLGA (Figure 19). Various acids were incorporated into the hydrogel to decrease the buffer capacity and allow PLGA degradation (Figure 19). The addition of 5% w/v humic acid resulted in approximately 40% release of dexamethasone in 30 days. The addition of 5% w/v acrylic acid and 5% w/v Nafion also increased the release rate, resulting in approximately 30% release in 30 days. Humic acid has a greater acid functionality per molecule than the other acids, explaining the higher release rate with this additive. The release rate of dexamethasone from the microspheres in the presence of the PVA gels and polyacid additives changes from biphasic to a zero-order release profile. This result is due to an alteration in the PLGA release rate within the gel and to the additional barrier of the gel itself once the drug is released from the microspheres. Through the use of different polyacids it is possible to tune drug release to achieve a desired release rate.

The addition of the various combinations of polymer/tissue response modifiers to implants provide an extremely simple, flexible and effective means to control the implant/tissue interface, improving implant lifetime and function. The close association of the tissue response modifiers overcomes the disadvantages of simple injection of the agent at the site of implantation, where blood flow or muscle movement alone can cause migration of the agent away from the site of implantation. For proteinaceous agents, which are particularly subject to degradation, the close association of the therapeutic agent with the implant can prevent significant loss of efficacy.

While preferred embodiments have been shown and described, various modifications and substitutions may be made thereto without departing from the spirit and scope of the invention. Accordingly, it is to be understood that the present invention has been described by way of illustration and not limitation.

What is claimed is:

1. An implant having a tissue/implant interface, comprising an implant having an outer surface; a bioactive polymer layer adjacent to at least a portion of the outer surface; and controlled release nanoparticles, liposomes, or microspheres containing a tissue response modifier, wherein the controlled release nanoparticles, liposomes, or microspheres provides the tissue response modifier to the site of implantation in a quantity effective to control tissue response at the site of implantation.
2. The implant of claim 1, wherein the bioactive polymer layer is self-assembled with metal cations.
3. The implant of claim 2, wherein metal cations are Fe^{3+} or Ca^{2+} .
4. The implant of claim 2, wherein the self-assembled bioactive polymer layer is a synthetic polymer.
5. The implant of claim 2, wherein the self-assembled bioactive polymer layer is a mussel adhesive protein.
6. The implant of claim 2, wherein the self-assembled bioactive polymer layer is assembled from humic acid.
7. The implant of claim 1, wherein the bioactive polymer layer comprises glutamic acid.
8. The implant of claim 1, wherein the bioactive polymer layer further comprises covalently bound poly(ethylene oxide), phosphatidyl choline, polyvinyl alcohol, polyethylene imine, an adhesive ligand, or a combination thereof.

9. The implant of claim 1, wherein the bioactive polymer layer comprises a hydrogel.

10. The implant of claim 9, wherein the hydrogel is polyvinyl alcohol.

11. The implant of claim 10, wherein the hydrogel further comprises acrylic acid, humic acid, nafion, or another polymeric acids, or combinations comprising at least one of the foregoing acids.

12. The implant of claim 1, wherein the implant further comprises an additional bioactive polymer layer.

13. The implant of claim 12, wherein the additional bioactive polymer layer comprises a hydrogel.

14. The implant of claim 1, wherein the bioactive polymer layer is formed by the polymerization of 2-hydroxyethyl methacrylate, a fluorinated acrylate, acrylic acid, methacrylic acid, or a combination comprising one of the foregoing monomers with an ethylenically unsaturated co-monomer.

15. The implant of claim 1, wherein the bioactive polymer layer is formed by copolymerization of 2-hydroxyethyl methacrylate with hydroxypropyl methacrylate, N-vinyl pyrrolidinone, 2-hydroxyethyl acrylate, glycerol methacrylate, n-isopropyl acrylamide, N,N-dimethylacrylamide, glycidyl methacrylate, or a combination thereof.

16. The implant of claim 1, wherein the bioactive polymer layer is formed by copolymerization of 2-hydroxyethyl methacrylate, N-vinyl pyrrolidinone, and 2-N-ethylperfluorooctanesulfanamido ethyl acrylate in the presence of EGDMA.

17. — The implant of claim 1, wherein the tissue response is inflammation, fibrosis, fibroblast formation, fibroblast function, cell proliferation, neovascularization, cell injury, cell death, leukocyte activation, leukocyte adherence, lymphocyte activation, lymphocyte adherence, macrophage activation, macrophage adherence, thrombosis, neoplasia, protein
5 adhesion to the implant, or a combination comprising at least one of the foregoing responses.

18. The implant of claim 1, wherein the tissue response modifier comprises an anti-fibrotic agent, steroidal anti-inflammatory agent, non-steroidal anti-inflammatory agent, anti-proliferative agent, cytokine, cytokine inhibitor, growth factor, vascular growth factor, neutralizing antibody, adhesive ligand, hormone, cytotoxic agent, or a combination comprising at least one of the foregoing tissue response modifiers.

19. The implant of claim 1, comprising a tissue response modifier which affects inflammation.

20. The implant of claim 1, comprising a tissue response modifier which affects neovascularization.

21. The implant of claim 1, comprising a first tissue response modifier which affects inflammation and a second tissue response modifier which affects neovascularization.

22. The implant of claim 1, wherein the tissue response modifier comprises 2-(3-benzophenyl)propionic acid, 9-alpha-fluoro-16-alpha-methylprednisolone, methyl prednisone, fluoroxyprednisolone, 17-hydroxycorticosterone, cyclosporin, (+)-6-methoxy- α -methyl-2-naphthalene acetic acid, 4-isobutyl- α -methylphenyl acetic acid, Mitomycin C, transforming growth factor alpha, anti-transforming growth factor beta, epidermal growth factor, vascular endothelial growth factor, anti-transforming growth factor beta antibody, anti-fibroblast antibody, anti-transforming growth factor beta receptor antibody, arginine-glycine-aspartic acid, REDV, or a combination comprising at least one of the foregoing tissue response modifiers.

23. The implant of claim 1, wherein the controlled release microspheres comprise PLGA.

24. The implant of claim 1, wherein the controlled release microspheres comprise predegraded PLGA microspheres.

25. The implant of claim 1, wherein the controlled release microspheres comprise PEG-treated microspheres.

26. The implant of claim 26, wherein the controlled release microspheres comprise a mixture of standard and predegraded microspheres.

27. The implant of claim 1, wherein the controlled release microspheres further comprise PEG-treated microspheres.

28. The implant of claim 1, wherein the site of implantation is the gastrointestinal tract, biliary tract, urinary tract, genital tract, central nervous system or endocrine system.

29. The implant of claim 1, wherein the site of implantation is at blood vessels, bones, joints, tendons, nerves, muscles, the head, the neck, or organs.

30. The implant of claim 1, wherein the implant is a material, a prostheses, an artificial organ, a repair device, an implantable drug delivery system, or a biosensor.

31. A controlled release delivery system, comprising a mixture of predegraded and untreated microspheres.

32. The controlled release delivery system of claim 31, wherein the microspheres comprise PLGA.

33. The controlled release delivery system of claim 31, wherein predegraded microspheres are made by stirring standard microspheres in a solvent for a time sufficient to produce a rough surface of the microsphere.

5 34. The controlled release delivery system of claim 31, further comprising PEG-treated microspheres.

10 35. The controlled release delivery system of claim 31, wherein the tissue response modifier comprises an anti-fibrotic agent, steroidal anti-inflammatory agent, non-steroidal anti-inflammatory agent, anti-proliferative agent, cytokine, cytokine inhibitor, growth factor, vascular growth factor, neutralizing antibody, adhesive ligand, hormone, cytotoxic agent, or a combination comprising at least one of the foregoing tissue response modifiers.

36. The controlled release delivery system of claim 31, wherein the tissue response modifier comprises 2-(3-benzophenyl)propionic acid, 9-alpha-fluoro-16-alpha-methylprednisolone, methyl prednisone, fluoroxyprednisolone, 17-hydroxycorticosterone, cyclosporin, (+)-6-methoxy- α -methyl-2-naphthalene acetic acid, 4-isobutyl- α -methylphenyl acetic acid, Mitomycin C, transforming growth factor alpha, anti-transforming growth factor beta, epidermal growth factor, vascular endothelial growth factor, anti-transforming growth factor beta antibody, anti-fibroblast antibody, anti-transforming growth factor beta receptor antibody, arginine-glycine-aspartic acid, REDV, or a combination comprising at least one of the foregoing tissue response modifiers.

37. A tissue/implant interface comprising the controlled release delivery system of claim 31.

APPARATUS AND METHOD FOR CONTROL
OF TISSUE/IMPLANT INTERACTIONS

Abstract

A tissue/implant interface, comprising an implant and a bioactive polymer layer adjacent at least a portion of the outer surface of the implant, wherein the polymer layer contains at least one tissue response modifier covalently attached to the polymer layer or entrapped within the polymer layer in a quantity effective to control the tissue response at the
5 site of implantation. Preferably, the at least one tissue response modifier controls inflammation, fibrosis, and/or neovascularization. Exemplary tissue response modifiers include, but are not limited to, steroidal and non-steroidal anti-inflammatory agents, anti-fibrotic agents, anti-proliferative agents, cytokines, cytokine inhibitors, neutralizing
10 antibodies, adhesive ligands, and combinations thereof. Use of the various combinations of tissue response modifiers with bioactive polymers provides a simple, flexible and effective means to control the implant/tissue interphase, improving implant lifetime and function.